### **Instruction Manual**

RT 200 Temperature Control Apprts. with Experiment Panels







### **Instruction Manual**



04/98



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#### 1 Introduction

The G.U.N.T. RT 200 Temperature Control Apparatus with Experiment Panels is used for experiments on simple temperature control. A soldering iron equipped with a thermocouple is used as the heater element. The temperature can be read on a digital display with a transducer. In addition there is a bar display for the indication of the temperature.

The system is equipped with a digital **industrial** controller.

An actuator regulates the **control variable**, that is the **power** to the soldering iron.

In this way experiments can be performed on all continuous control systems such as P, PD, PID and PI controllers, as well as on discontinuous controllers, such as 2-point controllers.

All components in the control loop are fitted to boards and can be hung in a support provided.

The student can become familiar with the components of a control loop, interconnect the components and vary the parameters.

The Appendix to this instruction manual contains working sheets that ease the evaluation of the experiments. All components are of a sturdy design and therefore well suited for student experiments.

Using the system, the following **topics** can be addressed:

- Layout of control loops
- Comparison of different types of controller
- Features of different control loops
- Components of a control loop



- 2 Unit Description
- 2.1 Unit Layout



Fig. 2.1

- Unit Layout (a different arrangement of the components is possible)
  - Table support (1)
  - Actuator component (2), with connection for control loop
  - **Control loop** component (3) with heated space shown, soldering iron as heater element, thermo-couple and Cu/stainless steel cooling plates
  - Controller component (4) with RS 485 interface
  - Bar display (5) for the control variable
  - **Transducer** component (6) with digital temperature display



Mains cable, connecting cable and thermocouple cable for the connection of the control loop as well as various laboratory cables (not shown)

### 2.2 Components

### 2.2.1 Control Loop



The objective of a temperature control system is maintain the temperature in a defined space (1) as constant as possible. For this purpose a heater is required, (simulated by soldering iron (2)), as well as a thermocouple (3) for the measurement of the temperature in the space.

The power supply (control variable) for the heater is provided via a 220V socket (4).

The thermocouple can be connected to a socket (5) on the transducer using the cable supplied.

To simulate a disturbance variable, cooling plates (6, copper and stainless steel) can be hung on the bolt to dissipate heat. Attention! Ensure that the plate (6) is lying exactly on the tip of the soldering iron (2)!

### 2.2.2 Controller



The **controller** (1) is an industrial unit. It is already pre-configured in the factory. For detailed information on the operation of the controller (scaling, etc.) please refer to the controller manual.

The controller is switched on using the **main** switch (2).

The actual value x (the temperature in the space) can be fed to the sockets (3) as a voltage of 0-10V (3), or the actual value can be connected directly to the thermocouple using socket (4).



The controller can also process the actual value x in the form of a current signal from 0-20mA; the current signal must be connected to the sockets (5) using laboratory cables. It is thus possible to use any transducer and sensor.

The **setpoint w** for the temperature is set directly on the controller with the aid of the arrow keys (6).

The **control value y** (the input current) is available at sockets (7) and can be connected to the actuator.

Using an **RS 485 interface** (8) it is possible to transfer the actual value, setpoint and control value to a PC.

### 2.2.3 Transducer



The **transducer** converts the temperature signal from the thermocouple (0-400C) into a proportional voltage signal (0-10V). For this purpose the thermocouple must be connected to **socket** (1), the voltage signal is available at the **laboratory sockets** (2).

The board also has a **digital display** (3) for the temperature. The transducer is switched on using **main switch** (4).



### 2.2.4 Control Variable Display



The control behaviour of the controller can be demonstrated with the aid of the **bar display** (1) by injecting the signal for the control variable y (current signal for the actuator) with the aid of the **sockets** (2) and (3). The bar display is switched on at the **main switch** (4).

The **actuator** (1) is a power regulator that regulates the power to the **socket** (2) as a function of the control variable y (current signal 0-20mA). The current signal is fed to the **laboratory sockets** (3) using laboratory cables. The main supply is provided via the **socket** (4).

### **RT 200 Temperature Control Apparatus** with Experiment Panels IAMBUF 2.3 **Connection of the Components** Thermocouple Cable \$--0 Mains Cable $\triangleright$ 1.246 199,9 199,9 ₹**▼**▲⊃ 00:



2.4

Control Loop Block Diagram

• •

Fig. 2.8



Connecting the Boards

Laboratory Cable



### 2.5 Controller Operation



MANUAL / AUTO ChangeFor the controller to be able to perform its function, it must be set to the AUTO mode. This operating state can be achieved by operating the MANUAL / AUTO changeover switch. The MANUAL mode is indicated by the Man. indication.

In the manual mode the actual value is displayed in the top line of the display in C (0-400 C). The setpoint is displayed in the bottom line. The actual value is proportional to the current input signal (0-20mA). I. e., an indication of 200 C corresponds to a signal of 10 mA.

In the manual mode the output signal can be adjusted using the two arrow keys.



### 2.6 Controller Configuration for Continuous Operation (P, PI, PD, PID controller)



Fig. 2.11

The power regulator is operated with the aid of the built-in controller. The control variable input at the power regulator is a continuous signal (analogue signal) of 0 - 20 mA, where 0 mA corresponds to no power and 20 mA corresponds to full power.

The controller has two different operating modes. Continuous control in which the output of the controller (OUT1) produces a continuous signal, and 2-point control in which the output of the controller (OUT2) produces a switching signal (relay).

The controller can be configured for the related task using the keypad on the front. For this purpose, proceed as follows:

Press the c key for more than 3 sec.

Change to parameter level, "Para" flashes.

Accept with 1x

2.6.1 Control Type



Fig. 2.12

Press the  $\bigcirc$  key for more than 3 sec.

Change to the configuration level, "Conf" flashes.



Change **CON1** to **10.0.0**, for this purpose press



and change the related value using



Using and "END/EXIT" change to the next level up.



### 2.6.2 Input Configuration



**C.201 x0 0 C.201 x0 0 C.201** 



Fig. 2.15

By pressing the increment key A change to **C.200** to configure input 1.

Change **INP1** to **30.0.2**, for this purpose press 1x

and change the related value using



Using and "END/EXIT" change to the next level up.

By pressing the increment key A change to **C.201** or **C.202** to scale input 1. Change **x0** to **0** 

Change **x100** to **400** 

Here other values may also be useful.

E.g. when using pressure transmitters

0 - 6 bar: x0=0; x100=6

0 - 100 mbar: x0=0; x100=100

### 2.6.3 Output Configuration



Change **OUT1** to **01.1.2**, for this purpose press 1x

and change the related value using

 $\bigcirc$ 







Fig. 2.17

### Leave the configuration level by using 🔽 🔺 to



choose END/EXIT and accepting using  $\square$  . "WAIT" appears.

Once the configuration level for the continuous mode has been set, a few values need to be changed in the parameter level.



#### Parameter Level



Fig. 2.18



Fig. 2.19



Fig. 2.20

Press the  $\bigcirc$  key for more than 3 sec.

Change to parameter level, "Para" flashes.

Accept using 1x Setpt." appears.

Set lower setpoint limit w0.

Change **w0** to **0**, for this purpose press 1x



Using and "END/EXIT" change to the next level up. Then set the upper setpoint limit **W100**.

Change w100 to 400, for this purpose press 1x  $\bigcirc$ 

and change the related value using



Using and "END/EXIT" change to the next level up. "Setpt." appears.



### 2.7 Controller Configuration for the 2-Point Controller



This configuration must be selected if you want to use a two-point controller.

Press the Ckey for more than 3 sec.

Change to parameter level, "Para" flashes.



### 2.7.1 Control Type



Fig. 2.22

Press the  $\bigcirc$  key for more than 3 sec.

Change to the configuration level, "Conf" flashes.



Change CON1 to **02.0.0**, for this purpose press 1x

and change the related value using

	1

Using and "END/EXIT" change to the next level up.

The rest of the procedure is similar to that for the continuous controller.

### 2.8 Setting the Controller Parameters Kp, Tn and Tv

Please refer to the controller operating instructions included.



### 3 Safety Instructions







- DANGER! Never open instructional board housing! There is a risk of electric shock!
- DANGER! Never touch tip of soldering iron with bare hands!
   There is a risk of burns!
- DANGER! Do not place cooling plates on plastic coated surfaces after use!
   The surfaces may be irreparably damaged
- ATTENTION! With cooling plates fitted do not exceed a temperature of 180C! There is a risk of overheating the instruction board material.

ATTENTION



### 4 Fundamental Principles of Control Technique

4.1 The Control Circuit

The structure of a control circuit should be explained by means of a level control. The control circuit mainly consists of:

- Controlled system, here the vessel
- Controller, here a industrial controller

The following are also present:

- **Fill level measuring device** for measuring the height of the fill level for example a diff. pressure transmitter
- Control valve for influencing the intake flow

All components are clearly displayed in a **control circuit diagram**.



Variables in the control circuit

- Actual value x: Fill level in cylinder
- Setpoint w: Desired fill level
- Manipulated variable y: Output variable of the controller

### **Control circuit diagram**



**Disturbance variable z:** Change in drain flow through ball valve

### 4.2 Principle behind a control system

The basic principle behind a control system is to have the output variable (**actual value x**) of an apparatus (controlled system) be kept to a certain value independent of disturbing influences. To do this, the **actual value x** is measured and referenced with the desired value (**target value w**). If a difference is found, the controller attempts to control the controlled system using **control output y** according to a certain control function, in order to cause the **actual value x** to approximate the **target value w** again.



d target With reference to the fill level control system

- Measure the fill level in the fill level cylinder
- Reference the current fill level with the desired target value
- If the fill level is too low, the controller increases the intake via the control valve
- If the fill level in the cylinder has reached the desired height, the intake flow is reduced
- If the fill level is too high, the controller throttles the intake until the desired fill level has been attained

This control process is continuous.



### 4.3 System parameters from the step response



The properties of the controlled system must be known for optimal adjustment of the controller to the controlled system. If the controlled system is unknown or cannot be expressed mathematically, the most important system parameters should be determined by experimental means.

In this test the unknown **reaction of the system** to a known step at the input is measured. The system demonstrates a **time response characteristic** for the dynamic and static properties at the output.

A differentiation is always made between two types of system depending on the characteristics of the step response.

In the first type of system, the output of the system reaches an upper range value after a certain period of time following introduction of an input step. This type of system is called a **self-regulating system**.

In the second type of system the output of the system does not reach a stationary upper range value after introduction of a input step, instead it heads towards infinity. This type of system is called a **system without self-regulation**.

х

y

х

У



self-regulating

without self-regulation

In the case of **self-regulating systems** a **stationary state** sets in after a certain period of time. The output of the system attains the upper range value  $x_s$ .





The **system parameters** can be determined from this time response.

- Proportional-action coefficient Ks
- Dead time Tt
- Delay time Tu
- Compensation time Tg

The **proportional-action coefficient Ks** reflects the static response characteristic

$$K_{s} = \frac{x_{s} Y}{y_{s} X}$$

where

- e ys manipulated variable step
  - x<sub>s</sub> stationary upper range value of the system output
  - Y maximum manipulated variable
  - X maximum output variable of the system

The **dead time T<sub>t</sub> (time lag)** indicates the delay with which the system output reacts to the input step.

The **delay time T<sub>u</sub>** shows the influence of a higher system order.

The **compensation time**  $T_g$  is a measure of the system lag.

The delay time  $T_u$  and the compensation time  $T_g$  are determined by applying a tangent at the point of the greatest slope in the step response. The distance from the first measurable reaction of the system to the point of intersection of tangent/zero line results in the delay time  $T_u$ . The distance from the point of intersection tangent/zero line to the point of intersection tangent/zero line to the point of intersection tangent/stationary upper range value results in the compensation time  $T_g$ .



#### 4.3.2 System without self-regulation



A differentiation should be made between two cases below with regard to a system without selfregulation

- The stationary upper range value of the control variable is outside of the admissible limit and is **infinite**.

Here, the system features **integral action**. Even with very small input variables, the output will ultimately be infinite.

In the case of the training stand this response can be achieved by closing the drain.

- The stationary upper range value of the control variable is outside of the limit yet still has a **finite** value.

Here, the system features  $PT_1$  action with a large system gain  $K_s$ .

In the case of the training stand this action is achieved by completely opening the intake and the drain.

The slopes of the step response of two different points of time with a distance t are used to determine these parameters. If  $PT_1$  action is assumes the following applies

$$\dot{\mathbf{x}} = \frac{\Delta \mathbf{x}}{\Delta t} = \frac{\mathbf{K}_{s} \cdot \Delta \mathbf{y}}{\mathbf{T}_{g}} \mathbf{e}^{-\frac{\mathbf{t}}{\mathbf{T}_{g}}}$$

 $\Delta x_2$ 

ys

time

 $\Delta t_2$ 

 $\Delta x_1$ 

Δt<sub>1</sub>



Two measurements result in the following relationship

$$\frac{\dot{\mathbf{x}}_{1}}{\dot{\mathbf{x}}_{2}} = \frac{\Delta \mathbf{x}_{1} \ \Delta \mathbf{t}_{2}}{\Delta \mathbf{x}_{2} \ \Delta \mathbf{t}_{1}} = \mathbf{e}^{\frac{\mathbf{t}}{\mathsf{T}_{g}}}$$

This results in the compensation time

$$\mathsf{T}_{\mathsf{g}} = \frac{\mathsf{t}}{\mathsf{In}\left(\frac{\Delta \mathsf{x}_{1} \ \Delta \mathsf{t}_{2}}{\Delta \mathsf{x}_{2} \ \Delta \mathsf{t}_{1}}\right)}$$

The system gain is calculated as follows

$$K_{s} = \frac{\Delta x_{1} T_{g}}{y_{s} \Delta t_{1}}$$



Х

y'



### 4.4 Comparison of different types of controllers

#### 4.4.1 Controller response characteristics

w-x

Kp=1/xp

The controller used in this training stand is a continuous controller which features P, PI, PD or PID action.

The response characteristics of the controller is determined by several parameters. In the most common case of a PID controller it is:

Proportional-action range x<sub>p</sub> (proportional action)

 Integral-action time T<sub>n</sub> (integral-action)

**Derivative-action time Tv** (differential action)

The output signal of the controller can be described as the sum of output signals of various transfer blocks with these various time characteristics.

The same input signal is applied to the inputs of all transfer blocks, namely the control difference w-x.

The characteristics of the various types of controllers are described in the following.





Time constant Step response



### 4.4.2 Proportional-action controller (P)

The P controller is the simplest type of controller. The manipulated variable is directly proportional to the **system deviation w-x**.

$$y = K_p \cdot (w - x)$$
 where  $K_p = \frac{100\%}{x_p}$ 



The remaining system deviation is a disadvantage. It is the inevitable result of the control function: since the manipulated variable usually does not vanish, the control deviation can also not vanish.

The remaining system deviation can be reduced by increasing the **gain**  $K_p$  or by reducing the **proportional-action range**  $x_p$ . However, the tendency of the control system to oscillate simultaneously increases when this is done. It can become unstable.

#### 4.4.3 Proportional-plus-differential controller (PD)

In the PD controller a **component proportionate to the speed** is fed back in addition to the P-component. This has a **damping influence**. As a result, a higher gain  $K_p$  can be selected without the system beginning to oscillate

$$y = K_p \cdot \left( (w-x) + T_v \frac{d(w-x)}{dt} \right)$$
  
where  $K_p = \frac{100\%}{x_p}$ 

The proportional-plus-differential controller thus has a smaller residual system deviation in general.





### 4.4.4 Proportional-plus-integral controller (PI)



In PI-controllers an integral component is fed back in addition to the proportional component. This prevents a lasting system deviation. As soon as the system deviation is not equal to zero, the integral part adds the deviations over time and the output variable of the controller increases continuously.Finally, the output variable is exactly so large that the **system deviation is equal to zero**.

$$y = K_p \cdot \left( (w-x) + \frac{1}{T_n} \int (w-x) dt \right)$$
  
where  $K_p = \frac{100\%}{x_p}$ 

The integral component reduces the stability and the P-component must be reduced accordingly.

### 4.4.5 Proportional-plus-integral-plus-differential controller (PID)

PID controllers are the most common type of controller. The manipulated variable is calculated from the **system deviation w-x** as follows:

$$y = K_p \cdot \left( (w-x) + \frac{1}{T_n} \int (w-x) dt + T_v \frac{d(w-x)}{dt} \right)$$
  
where  $K_p = \frac{100\%}{x_p}$ 

Thanks to the integral component this type of controller, just as the PI controller, has no remaining system deviation.

The differential component is proportionate to speed and, therefore, has a damping effect.



PID controller



### 4.5 Controller setting according to ZIEGLER-NICHOLS



Increasing the gain step by step

The setting rules according to ZIEGLER-NICHOLS are a commonly used and proven method of adapting a controller to a system.

The advantage of this method is that the system parameters do not need to be known explicitly. The necessary information concerning the system is gained from the response of the closed control circuit at the limit of stability.

To do this, the controller is configured as a pure **P controller** and the gain  $K_p$  is increased so much or the proportional-action range is reduced until the control circuit just begins to oscillate.

The critical gain required for this  $K_{p \text{ crit}}$  or  $x_{p \text{ crit}}$  and the cycle time  $T_{crit}$  of the sustained oscillation to be employed are used to determine the controller parameters.

The controller parameters for a PID controller are then calculated as follows

Controller parameters according to Ziegler-Nichols			
Type of controller	Р	PI	PID
Proportional range <b>x</b> p	2.0 x <sub>p crit</sub>	2.2 x <sub>p crit</sub>	1.66 x <sub>p crit</sub>
Integral-action time <b>T</b> n	-	0.85 T <sub>crit</sub>	0.50 T <sub>crit</sub>
Derivative-action time $T_{\nu}$	-	-	0.12 T <sub>crit</sub>

tolerance

band



#### 4.6 Evaluating the control quality

The control quality is evaluated using the step response of the closed control circuit.

A differentiation is made here between the response to setpoint changes and the response to disturbances.

- The **response to setpoint changes** describes the reaction of the control circuit to a change in the target value.
- The **response to disturbances** reflects the influence of disturbances on the actual value.

In order to interpret the step responses in a comparative manner several characteristic values are introduced.

#### Overswing amplitude xo

The overswing amplitude is a brief deviation of the actual value from the target value. It is a measure of the tendency of the control circuit to oscillate with regard to damping.

#### Remaining system deviation e=w-x

The remaining system deviation is a static value. It is a measure of the accuracy of the control system (bottom illustration). It is of particular significance for P and PD controllers.

Overswing amplitude and remaining system deviation are often referred to in relation to the target value and are indicated in percentages.

#### Rise time Ton

The rise time is a measure for the speed of the control process. It is the time between the target value step and the first attainment of the tolerance band.

x,w









Response to disturbances

In the case of response to disturbances, the rise time is the time between the first deviation from the tolerance band and reentering the **tolerance band**.

If the actual value has a remaining system deviation which is too great (response to setpoint changes bottom illustration), then it is the time until first attainment of the later stationary upper range value.

#### Settling time Toff

The settling time reflects the time form the target value step until the final settling of the actual value in the tolerance band.

In the case of response to disturbances, the time between first leaving the tolerance band and final settling in the tolerance band applies. The relationship between the rise time and the settling time is itself a measure for the damping of the control circuit. A small rise time with a large settling time means small damping and tendency to oscillate.



#### 4.7 Cascade control

This special type of control with an auxiliary controlled variable uses two controllers connected in series. The control device consists of a **master controller** and a **follow-up controller**.



At the input of the master controller, the controlled variable  $x_1$  is compared with the reference variable  $w_1$  and the control difference  $e_1$  is formed. Its output variable, the control signal  $y_1$ , acts as a reference variable  $w_2$  for the follow-up controller, and is compared at its input with the auxiliary controlled variable  $x_2$ . By dividing the control circuit into a follow-up control circuit and a master control circuit, the quality of control of  $x_1$  is improved. In case of a fault, since the change in  $x_2$  occurs earlier, the follow-up controller triggers a control process, thereby supporting overall control.

In general, control momentum can be improved via the introduction of subordinate control loops in the control circuit.



### 4.8 On-off Controller





**Two-point controllers** are among the simplest types of controllers. They are used, for example, as thermostats in furnaces and air conditioning systems.

Two-point controllers are **switches** which only have two states, dependent on the input signal; **On**: y=100% and **Off**: y=0%. In general, the two-point controller does not switch exactly at x = w, rather with a certain **hysteresis** at  $x = w \pm x_{sd}/2$ . This results in the depicted curves for the control and manipulated variables. The **manipulated variable y** is **pulse-width modulated** and has a **period T** of

$$T = t_e + t_a$$

The **manipulated degree**  $\alpha$  of the controller is the result of the **switching ratio** 

$$\alpha = \frac{t_e}{t_e + t_a}$$

these two characteristic variables of the two-point controller are dependent on the set hysteresis on the one hand and on the system parameters  $K_s$ ,  $T_t$  and  $T_g$  on the other.

The **amplitude x**<sub>0</sub> of the switching cycles can be approximated using

$$x_0 \approx \frac{x_{sd}}{2} + \frac{K_s Y}{2} \cdot \frac{T_t}{T_g}$$





Three-point controller with hysteresis

Another type of continuous controller is the **threepoint controller**. It is often used in motor drives. Its behaviour is similar to that of the two-point controller. In a drive, it can determine the direction of drive (clockwise or counter-clockwise) and standstill. In a temperature control, it produces three control states:

Heater ON, cooler OFF (heating)

Heater OFF, cooler OFF

Heater OFF, cooler ON (cooling)

The control states can also be referred to as 1, 0 and -1.



5 Experiments

### 5.1 Familiarisation with the Layout and Function of an Industrial Controller

The student should be given time to become familiar with the control loop on the system. For this propose there is a working sheet in the Appendix on which the related terms can be entered on a **diagram of the control loop**.

In addition, the student can become familiar with the **operation of the controller**. The operating instructions for the controller can be used for this purpose.

### 5.2 Comparison of Different Types of Controller

### 5.2.1 Preparation for the Experiment

In the following experiments are described that enable the student to compare the different controllers and their action.

For this purpose the controller must first be configured to the required type, as described in Sec. 2, and the parameters must be entered.

The following parameters provide typical step responses:



	P controller	PI controller	PD controller	PID controller	Two-point controller
Step from to	140 to 160 °C	220 to 240°C	240 to 260°C	200 to 220°C	260 to 280°C
Хр	10 %	15 %	5 %	20 %	10%
Tn	0	30 sec	0	20 sec	15 sec
Tv	0	0	5 sec	6 sec	5 sec

Tab. 5.1Good control parameters for typical controller behaviourNote: The two-point controller has a PID characteristic

### 5.2.2 Performing the Experiment

- Set **setpoint w** to the above mentioned start temperature on the controller.
- Wait until the temperature is reached
- Record initial measured values: Time t (=0 sec, measure using stopwatch), read control variable Y (current in mA or in %) on bar display, read actual value X (temperature in the heated space) at the transducer
- Enter step at the controller by adjusting the setpoint w to the above mentioned final temperature.
- Every 5-10 sec take **measurements** until a time or around 200 sec has passed.

### 5.2.3 Evaluation of the Experiment

If the values measured are plotted on a graph, the following diagrams are produced:



**RT 200** 





Based on the diagrams, the typical properties of the controller types can be confirmed:

- P controller: permanent temperature error be-\_ tween setpoint and actual value can be seen
- PD controller: damping can be seen (only one oscillation), less error than for the P controller
- PI controller: no error any more, but it is also not possible to see any stability (system oscillates)
- PID controller: no error and good damping
- Two-point controller: switching states can be clearly seen on the control value y, control is of adequate quality for this case

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#### 5.3 Introduction of a Disturbance

To investigate the behaviour of the controller types when there is a disturbance, a **disturbance variable** can be applied. For this purpose one of the cooling plates must be placed on the soldering iron.

The copper plate has a greater cooling effect than the stainless steel plate.

**ATTENTION!** The temperature must not exceed 180C because the plastic parts of the system may be irreparably damaged by the heat.

# RT 200 Temperature Control Apparatus with Experiment Panels



- 6 Appendix
- 6.1 Working Sheets
- 6.1.1 Temperature Control System Control Loop



RT 200	Temperature Control Apparatus
	with Experiment Panels



## 6.1.2 Data Recording

Controller Type :		Date:						
		Name:						
Parameter:	Xp =							
	Tn =							
	Tv =							
	Setpoint w =°C	Start temperature:°C						

#### **Measured Values:**

t in sec	X in mA	Y in °C	t in sec	X in mA	Y in °C

Notes :

RT 200 Temperature Control Apparatus with Experiment Panels



6.2 Tech	nical Data
----------	------------

<b>Temperature Control S</b>	System	
Heat Source: Soldering	iron	
Power	max. 16	W
Supply:	230 V / 50	Hz
(Optional alternatives, se	ee rating plate)	
Controller:		
Standard Input Signal:	0/4 20	mA
	0 10	V
٦	Thermocouple	
Standard Output Signal	0 20	mA
Operating Modes:		
Continuous control syste	em and	
two-point control system	1	
Controller Types: P, PI,	PD and PID co	ntroller,
Param	leters can be se	et
Display	digital, LED	
Supply:	230 V / 50	Hz
(Optional alternatives, se	ee rating plate)	
Temperature Transduc	er	
Signal Input 1	hermocouple	type k
Signal Output	0 10	VDC
Temperature Range	0 400	С
Display digital, 3	1/2 digit, LED	
Supply	230 V / 50	Hz
(Optional alternatives, se	ee rating plate)	
Control Variable Displa	ау	
Signal input	0 20	mA
Display LE	ED bar display	
Supply	230 V / 50	Hz
(Optional alternatives, se	ee rating plate)	
Actuator		
Input Signal	0 20	mA
Output Signal	0-16	W
Supply	230 V / 50	Hz
(Optional alternatives, se	ee rating plate)	

# RT 200 Temperature Control Apparatus with Experiment Panels



#### **Overall Dimensions**

(L x W x H):	700 x 350 x 700	mm
Weight:	approx. 38	kg

PMA Prozeß- und Maschinen-Automation GmbH



# Industrial controller KS92/94



DAC<sup>®</sup> is a patented method and a registered trademark of Regeltechnik Kornwestheim GmbH.

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ovc+/-)	10.0.2       S         16.6.3       S         106       S         16.6.4       S         16.6.5       S         OUTPT:       S         16.7.1       S         16.7.2       S         16.7.3       S         16.7.4       S         16.7.5       ig         16.7.6       D         ALARM:       S         16.8.1       A         16.8.2       A         16.8.3       A         16.8.4       A         TUNE:       DISP:       U         AUX:       A	ignal input 3 / IN ignal input 4 / IN ignal input 5 / IN ignal input 6 / IN  ignal output 6 / IN  ignal output 1 / C ignal output 2 / C ignal output 3 / C ignal output 4 / C gnal output 5 / OD OO5,6 (digital cor  larm 1 / (limit 1) larm 2 (limit 2) larm 3 (limit 3) larm 4 (limit 4) self-tuning Ser interface for Additional functio	IP3 (ratio v)         IP4 (variab)         IP5 (ratio v)         IP6 (auxilia)         OUT1         OUT2         OUT3         OUT4         OUT5	/ariable le x3, e /ariable ary var: 	x 2 0 ext. see able   	r aux         et-po         ext. s         Yp, f	et-pc eedb	y va /ext, int ack        	Wex Yp)	t)	e co		. 105 ol . 106 . 106 . 107 . 107 . 107 . 108 . 109 . 109 . 109 . 109 . 110 . 111 . 111 . 111 . 111 . 111 . 112 . 112 . 113

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## 1 General hints

Industrial controllers KS92 and KS94 belong to a new generation of microcomputer-based controllers in the upper performance class.

Despite their versatility, these controllers are easy to operate. Not only "slow" thermal processes, but also pressure and flow with short reaction times can be controlled without problems. Due to measuring and control functions configurable within wide limits, the controllers can be used for a wide range of application.

Safe, reliable control within close tolerances, and high plant availability are pre-requisites for economic production.

Controllers with reliable and robust control algorithms are the basis for stable process conditions, also with varying operating parameterses.

A self-tuning function ensures short start-up times. The "thinking" operator guidance system with standard symbols, plain-language texts plus software and hardware interlocks prevent operating errors and thus reduce downtimes.

Controllers KS92 and KS94 are configurable as signallers, 2-point, 3-point, 3-point stepping and continuous controllers. Moreover, the output functions can be configured for  $\Delta$ /Y/off, position control, split-range control and numerous 3-point combinations of switching/continuous control.

Control modes are set-point, set-point/cascade and programmer, each with the possibility of set-point offset. The effect of offset can be additive (e.g. reduced stand-by set-point) or a factor (e.g. O2 correction or split load).

Offset can be triggered by an external contact, whereby the value is defined via an analog signal or via an adjustable parameter.

Additional control modes:

- Ratio control (stoichiometric combustion, mixing ratios, additives, batching, ...)
- Three-element control (level control in a steam boiler, ...)
- Mean value calculation from two process values.

Apart from a correcting function for the measurement signal, it is possible to scale, linearize or square-root every input and output signal. This enables the controller to be matched precisely to the application without any supplementary equipment.

For every-day practice, feed-forward control has proved very useful to line out disturbances, e.g. with steam-generating plants. For applications where several controllers act on a single actuator, the output limiting function is recommended. Alternatively, preset output limits can be used. This not only applies for continuous outputs, but also for switching and three-point stepping outputs (motor control).

#### 1.1 Technical data

The technical data are given in data sheet no. 9498 737 28333.

#### 1.1.1 Safety notes

#### Following the enclosed safety instructions 9499 047 07101 is indispensable!

The insulation of the instrument conforms to EN 61 010-1 with pollution degree 2, overvoltage category III, operating voltage 300 V and protection class I. Additional with horizontal installation, a protection to prevent live part, e.g. wire ends, from dropping into the open housing of a withdrawn controller must be fitted.

#### 1.1.2 Electromagnetic compatibility

The instrument conforms to **European Directive 89/336/EEC** and will be provided with the CE-marking. The following European Generic Standards are met: **Emission: EN 50081-2** and **Immunity: EN 50082-2**. The unit is suitable for use in industrial areas (in residential areas, RF interference may occur). The electromagnetic radiation can be reduced decisively by installing the unit in a grounded metal switch cabinet.

#### 1.1.3 Maintenance / Behaviour in case of trouble

The controller needs no maintenance. The rules to be followed in case of trouble are:

- Check mains (voltage, frequency and correct connections),
- check, if all connections are correct,
- check the correct funktion of the sensors and final elements,
- check the configuration words for required functions and
- check the adjusted parameters for required operation.

If the controller still does not work properly after these checks, shut down the controller and replace it.

**Cleaning:**Housing and Front can be cleaned by means of a dry, lint-free cloth. No use of solvents or cleansing agents!

#### 1.1.4 Electrical connections

- The electrical connections must be made according to the connecting diagram. For R.F. interference suppression, the mains cables must be kept separate from all other cables.
- The protective earth, which is to be taken to terminal A11 (P13 with continuous controllers) must be grounded via a lead which should be as short as possible (15 cm during test).
- When connecting a contactor to the relay output, an RC protective circuit is required to prevent high voltage peaks which might cause trouble to the controller.

# 2 Mounting and connection

#### 2.1 Mounting

The mounting position of controllers KS92 and KS94 is uncritical. Sufficient space for mounting should be provided on the rear of the control panel.

The controller mounting procedure is as follows:

- Mark and realize the panel cut-out as shown in the drawing below.
- Insert the housing into the panel cut-out from the front.
- Fit a fixing clamp to the controller top so that it locks into one of the housing cut-outs. Tighten it slightly using a screwdriver.
- Fit the second fixing clamp accordingly on the controller bottom, in diagonal position to the upper fixing clamp.
- Tighten the two fixing clamps, until the housing is seated firmly without distortion.

For reaching **protection type IP65** between controller and panel, an additional sealing ring must be provided. Moreover, two further fixing clamps are required. The mounting material required for this purpose can be delivered on request.



**S.I.L. switch:** with the switch closed, transition to parameter and configuration level is disabled. When making an attempt to change over to the parameter level, "**ParaL**" is displayed (text1). Correcting variable, set-point and parameters at the "extended operating level" remain available for selecting and changing. For access to the S.I.L. switch, release the locking screw and withdraw the instrument module from the housing. Subsequently, re-insert the controller module into the housing and mount it with screws.

**Caution!** The instrument contains ESD-hazarded components.



#### Removing the controller from the housing 2.1.1

For maintenance and service purposes, the controller module can be removed from the housing, whereby the housing with the relevant wiring remains in the installation.



If the operating voltage is switched on during this procedure, the live terminals in the controller housing must be protected against contact.



The controller electronics contains electrostatically sensitive components. Static discharge must be prevented by suitable measures.

When removing several controllers, take care that the controllers are re-mounted into the correct housings! For this, not only the hardware, but also the data configured in the controller are decisive.

For dismounting the controller module from the housing, remove the captive screw on the controller front. Hereby, the module is released from the housing, until it can be removed.

#### 2.1.2 Installing the controller in the housing

Note that each specific controller module belongs to a particular housing.

Insert the module carefully into the housing guide rails in the correct mounting position and slip it in position without pressure. A small remaining gap between front and frame is correct. Tighten the screw on the controller front, until the module is firmly locked in position.

# **3** Electrical connections

The electrical connections must be made according to the connecting diagram. For R.F. interference suppression, the mains cables must be kept separate from all other cables.

The protective earth, which is to be taken to terminal A11 (P13 with continuous controllers) must be grounded via a lead which should be as short as possible (15 cm during test).

When connecting a contactor to the relay output, an RC protective circuit is required to prevent high voltage peaks which might cause trouble to the controller.

The controller is provided with flat-pin connectors 1 x 6,3 mm or 2 x 2.8 mm for electrical connection.

#### **Connecting diagram:**

galvanic isolation



\* Versions with integrated supply voltage (connection example look at page )

### 3.1 Supply voltage connection **(5)**

The following controller versions are available:

#### AC versions

 90...260 V AC (KS92 only 230 V AC) Frequency: 48...62 Hz Power consumption: approx. 10 VA

#### 24 V UC versions (only KS 94)

- 24 V AC, 48...62 Hz The voltage limits are 24 V AC. (+10...-15 %)
- 24 V DC With the 24 V DC version, the limits are within 19,2 and 30V.

#### 3.2 Connecting the analog inputs INP

#### Input INP1 1

X1 Input for variable x1. (see page 31 ff)

- a Thermocouple
- **b** Resistance thermometer (PT100 in 3-wire connection)
- **c** Temperature difference as 2 PT100 in 2-wire connection
- **d** Potentiometric transducer
- e Current
- f Voltage

#### Input INP3 🕞

Dependent of configuration, this input is used for variable x2 or variable z. The reference potential (GND) of this input is at terminal C10 (see page 34).

#### Input INP4 🕞

23 Dependent of configuration, this input is used for variable x3, external set-point or override control (OVC). The reference potential (GND) of this input is at terminal C10 (see page 34).

#### Input INP5 🕄

This input is used for variable x2, for the external set-point or for external set-point 4 offset (configuration level **L**. **180**).





#### Input INP6 **2**

This input is used for position feedback with 3-point stepping controllers, for the external set-point or for the external set-point offset (configuration level L. **(BD**) (see page 35)

## 3.3 Outputs OUT

#### Output OUT1 7

Dependent of version, OUT1 is a continuous, a logic or a relay output. It may be allocated to Y1 or to alarm. With logic and continuous output, a protective earth must be connected to P13. The logic signal switches between 0 and 20 mA (load  $\leq 600 \Omega$ ) or 0 / > 12 V (load  $\geq 600 \Omega$ ) (see page 34).

#### Outputs OUT2, OUT4 and OUT5 6

These outputs are relay outputs. Output OUT2 is configured either for y2 or for alarm (see page 38). Outputs OUT4 and OUT5 are allocated to alarms LIM1 / LIM2.

With programmers, they can be configured in addition to outputs 1...4 or for program end (**E.590** / **E.59** () (see page 38).

#### Output OUT3 (6)

Dependent of configuration, OUT3 is a continuous or a logic output. The logic signal switches between 0 and 20 mA (load  $\leq 600 \Omega$ ) or 0 and 12 V (load  $\geq 600 \Omega$ ).

Which signal shall be taken to this output must be determined at configuration level. Selection between various controller outputs, process values and set-point is possible (see page 37)

#### 3.4 Digital inputs di

#### Digital inputs di1 and di2 4

Dependent of configuration (**[. 190** and **[. 191**), inputs di1 and di2 can control the following procedures:

- Switch-over between internal set-point **W** (0) and externel set-point **Wext** (1)
- Switch-over between internal set-point **W** (0) and second set-point **W2** (1)
- Switch-over between automatic (0) and manual (1) operation
- Set-point offset switch-on; normal (0) offset (1)
- Switch-over between normal correcting value (0) and safety correcting value (1)
- Controller switch-ON (0) or OFF (1)
- Switch-over between PI (0) and P (1); with 2/3-point and continuous controllers or feedback switch-off with 3-point stepping controllers
- Bumpless switch-over between normal correcting value (0) and safe correcting value (1)
- Bumpless switch-over to internal set-point (tracking only di2) OFF (0) ON (1)

#### Digital inputs di3 to di12 9023

- di3 used for switch-over between local (0) and remote (1).
  - used for switch-over between program STOP (0) and START (1) (L192; SPrSt).
- di5 used for programmer RESET; normal (0), reset (1).

di6/di7

di4

used for program number selection with programmer.

di6	0	1	x
di7	0	0	1
Programm	1	2	3

	di8	0	1	0	1
	di9	0	0	1	1
,	Parameter set	0	1	2	3

di7/di8 used for program number selection with programmer.

di10 minimum delimitation of the correcting variable with 3-pnt.stepping controller

dill maximum delimitation of the correcting variable with 3-pnt.stepping controller and can be configured for switching on the effective set-point offset ( **L** 190 : 5dWon).

di12 switches over bumplessly to the internal set-point (tracking) OFF (0) ON (1). and can be used for switching over to the second set-point W2 (**L 190**) OFF (0) ON (1).

#### 3.5 Digital outputs do1 to do6 9 do1 indicates the status of control output 1 with programmer. do2 indicates the status of control output 2 with programmer. do3 indicates the status of control output 3 with programmer. indicates the status of control output 4 with programmer. do4 do5 indicates, if the controller is in manual or automatic mode, or the Y1 condition with switching controllers (**E.595**). indicates, if the controller uses the external or the internal set-point, or do6 status Y2 with switching controllers (**E.5**97).

#### 3.6 Versions with integrated supply voltage

The supply voltage can be used only for energization of a 2-wire transmitter or for energization of max. 4 control inputs. The supply voltage is potential-free and can also be used for energizing inputs INP3 ... INP6 or for other units. Selection of supply

voltage or digital inputs is by S.I.L.

switches (see figure opposite).



The supply voltage is only applied to

terminals A12 and A14 with INP1 configured for current or thermocouple ([.200; type) and the S.I.L. switches set for transmitter supply (factory setting)! With the S.I.L. switches set to digital input, the voltage is applied to terminals A1 and A4 independent of the configuration of input INP1. In this case, the voltage input of INP5 is not available.

Supply voltage for energization of digital input (e.g. di1...di4)

External use of the supply voltage





Connection of a 2-wire transmitter on example of INP1 or INP5



## 3.7 Connecting the bus interface **(1)**

TTL or RS422 or RS485, PROFIBUS or INTERBUS. With TTL, an interface module for conversion to RS422/RS485 is required. 4 units may be connected to an interface module.

#### 3.7.1 Operation

KS94 data can be read, or displayed and modified from the front-panel PC interface or via the serial interface.

After delivery of controller KS94, the PC interface is active. KS94 configuration and parameter setting are supposed to be done by means of the engineering tool before commissioning.

Switch-over to the serial interface is either

- via operator dialogue (front):
- or by activating 'REMOTE' (→ page 17). Switching back to LOCAL does not cause switch-over to the front-panel interface.

Switch-over to the PC interface is only possible with the R/L input set to LOCAL.

#### 3.7.2 Remote/local

Units with serial interface are fitted with a hardware input (di3) for switch-over between REMOTE and LOCAL operation (R/L).



During **'REMOTE'** all operations via the serial interface (writing and reading) are permissible. The following operations are still possible via the keys of the local operating front panel:

Display switch-over

Display of parameters without modification

Display of configuration data without modification

During remote operation, the PC interface cannot be operated. When switching over from LOCAL to REMOTE, an active PC interface is switched off.

		PROFIBUS interface
During 'LOCAL', only reading of all		
data via the serial interface is permissible.		front-panel interface
Modifications are not possible,		
exception:		
any data related only to the interface		
or which are not adjustable local		
via local operation.	front-panel operation	R/L input

### 3.7.3 Connection examples





Fig.: 2 RS422-interface connection





Fig.: 3 PROFIBUS-DP connection







# 4 Operation

4.1	Front view			
	Fig.: 6 Fron	t view		
	LED 2 e.g. Cool LED 1 e.g. Hea	ling O O O O O O O O O O O O O O O O	LED 3 e.g. Alarm 1 LED 4 e.g. Alarm 2	
	Locking screw		Display 1 e.g. Process value	
	Text 1 <i>e.g. phys</i> Text 2 <i>e.g. Barg</i> <i>Dialogue</i>	ical unit graph / Y: ••• 55%	Display 2 e.g. Set-point	
			Selection key	
	PC interface		Increment key (↑)	
	Manual/Automa	tic key	Decrement key $(\downarrow)$	
	Locking screw:	Locks the controller module in the housing.		
	LEDs:	indicate the status of controller outputs Y1, Y2 and alarms LIM1 LIM2 (other settings at configuration level <b>[.800</b> ).	,	
	Display 1:	indicates the process value at operating and parameter level, and the configuration code at configuration level.		
	Display 2:	indicates the set-point during automatic operation at operating level and the correcting value during manual operation. The values are adjustable directly with push-buttons $\blacksquare$ and $\blacksquare$ . Further displays can be adjusted by means of configuration code ( <b>EBD</b> $\ddagger$ ).		
	Text 1:	indicates the short-form dialogue or the unit of display 2. Further displays can be adjusted by means of configuration code ( <b>LBDD</b> ).		
	<b>Text 2:</b>	indicates the correcting variable bargraph. Further displays can be adjusted by means of configuration code ( $[.800]$ ).		
	PC interface:	PC connection for configuration, parameter setting and operation the engineering tool	by means of	
4.2	Status displa	vs		

#### 4.2

F	81	
•C Y: •••••	[]	5 <mark>8</mark> 60

This message signals a sensor error. Possible cause: Break or wrong polarity with thermocouple Break or short circuit with Pt100 and potentiometric transducer Break with 4...20mA and 2...10V standard signal

The following messages can be displayed in KS92/94 'Text1'.

ClockF	Faulty clock (real-time clock must be re-adjusted.)
Recov	Recovery function is active (after power recovery, the process is controlled with the correcting variable determined last.
Grw	Gradient function is active (the set-point changes at an adjustable (Grw+/-) rate of change).
Y2	The second correcting variable (safety correcting variable) is active
AdaF	Self-tuning was canceled with error.
Ada	Self-tuning busy
Timer	Timer function is active (a future starting point was not reached yet).
CalEr	Calibration error with automatic position feedback calibration.
Block	No motor actuator reaction (only with the DAC function activated).
DirEr	Faulty motor actuator output action (only with the DAC function activated).
-YFail-	Yp error (potentiometer defective or not connected (only with activated DAC function).

#### 4.3 Menus 1...3

Apart from the parameter and configuration words, the following dialogue words are used (Text1):

Те	ext1	Signification
CBus	CFrnt	PC communication via interface at terminals B12B16
Clear		The additional display selected at operating level is deleted ( $\rightarrow$ Mark)
Clock		Setting the clock
Conf		Transition to configuration level
End		Return to the previous selection menu
Exit		Return to operating level (main display)
Hold		The displayed parameter is determined as standard display.
Mark		The displayed parameter is stored as additional display at operating level $(\rightarrow Clear)$
More		The configuration level area described with MORE is accessible
OStar	OStop	Self-tuning is started or stopped
Para		Transition to parameter level
PRun	PStop	Programmer starting or stopping
PSet	PRes	Programmer preset or reset
Quit		Return to operating level (main display) without storage of the values changed last

#### 4.4 The operating level

#### If the set-point is set to '----' by means of $\mathbf{\nabla}$ , the controller is switched off!!

*Menu 1* is always selectable at operating level: deletion of additional display (Clear), communication interface switch-over (CBus  $\leftrightarrow$  CFrnt) and starting (OStar) or stopping (OStor) the self-tuning, setting the clock (Clock), operate the programmer (PRun  $\leftrightarrow$  PStor; PRes; PSet) and transition to parameter level (Para).





### **4.5** Parameter and configuration level

*Menu 1* is always selectable at operating level: several operations ( $\rightarrow$  7.2) and transition to parameter level (**Para**).

*Menu 2* is always selectable at parameter level: selection of additional displays (Mark), return to parameter level (End), return to operating level ( $E \times it$ ), transition to configuration level (Conf).

**Menu 3** is always selectable at configuration level: permitting the MORE area (More), return to configuration level (End), return to operating level without storage of the last changes (Quit) or with storage of the changes (Exit).



*Value adjustment* is as follows (parameter values / configuration codes):

- Fig.: 9 Example for a single parameter
- Fig.: 10 Example for combined data (e.g. C-Codes)





# **5** KS92/94 function survey

#### **5.1** Basic hardware functions

Various KS92/94 controller versions according to order number are available. Decisive for the hardware is the number of connected circuit boards, i.e. connectors.

A large number of standard applications can be realized only with the KS92/94 basic version, which contains circuit boards P and A. The input and output functions shown in the following correspond to the basic setting. Finally, however, the individual configuration is decisive:

#### 5.1.1 Circuit board P:

Output OUT1:	positioning signal OUT1 can be ordered as a current or relay output. Dependent of selected controller type, it can be operated as a continuous 0/420mA signal or as a 0/20mA logic signal.
Output OUT2:	positioning signal

	positioning signal
Output OUT4:	limit signal (alarm)
Output OUT5:	limit signal (alarm)

#### 5.1.2 Circuit board A

Universal input INP1:	process variable x1 (process value)
Difference input INP5:	external set-point We
Measurement input INP6:	Position feedback yp with 3-point stepping and continuous controller

Control input di1:	set-point switch-over
Control input di2:	automatic/manual switch-over

#### 5.1.3 Circuit board B (optional)

Circuit board B contains a serial interface (TTL or RS485; ISO1745- and MODBUS protocol), a real-time clock and additional control inputs and outputs, which are reserved exclusively for the programmer functions:

Control input di3:	"remote/local" mode
Control input di4:	programmer start/stop
Control input di5:	programmer reset
Control input di6:	program selection
Control input di7:	program selection
Control output do1:	control output 1
Control output do2:	control output 2
Control output do3:	control output 3
Control output do4:	control output 4

#### 5.1.4 Circuit board C (optional, only possible with KS94)

Circuit board C offers further configurable inputs and outputs.

Difference input INP3: Difference input INP4: Current output OUT3:	disturbance variable z or process variable x2 (ratio, three-element,) external set-point We, set-point offset dWe, override control OVC, process variable x3 (three-element), operating mode continuous 0/420mA or logic 0/20mA; function configurable
Control input di8:	selection control parameter set 14
Control input di9:	selection control parameter set 14
control input di10:	override control OVC+ with three-point stepping controllers
Control input di11:	override control OVC- or set-point correction dW(e) "On/off"
Control input di12:	w/W2 switch-over
Control output do5:	positioning signal y1 (switching controllers) or "A/M" status
Control output do5:	positioning signal y2 (switching controllers) or "i/e" status

### 5.2 Survey of included function modules

A survey of function modules and their interdependence is shown below. The individual function modules are described in the following sections.





### 5.3 Galvanic isolation

Galvanic isolation is necessary for safety (contact safety) and for measurement reasons.

Due to the KS92/94 electronics construction, galvanic isolation is standard without extra charge. A transformer in the power supply always isolates all inputs and outputs from the supply voltage. Data exchange between electronics p.c.b. A and power supply or output p.c.b. P is also galvanically isolated. I.e. positioning output **OUT1** which can be designed for 0/4...20 mA, is also isolated from all inputs. Control inputs **di**, control outputs **do** and serial interface are always galvanically isolated via opto-couplers, i.e. they cannot contribute to stray potential and error due to leakage current.

Although additional current inputs INP3 and INP4 of option C are galvanically connected (difference inputs; COMMON), they are isolated from the rest of the instrument. This also applies to current output OUT3.

This means: if hardware option C is used, process value, set-point and correcting variable can be galvanically isolated. Even an additional process value output OUT3 (0/4...20mA) is galvanically isolated from the input.

Common control signals as A/M, w/W2, int/ext, etc., e.g. signals coming from a PLC and in many cases without galvanic isolation, are handled with galvanic isolation and do not cause potential compensation. The same applies to control outputs **do**, which are connected electrically with control units, i.e. which imply a risk of potential connections.

In the connecting diagram on page 13, the double lines clearly show the galvanic isolations throughout the controller.

Galvanic isolation of inputs and outputs is shown in the following drawing.



KS94

#### 5.4 Input conditioning

Before the pre-filtered (time constant ...; limiting frequency ...) analog input signals are available as digitized measurement values with physical unit and can be used e.g. as process value, set-point or position feedback, they undergo extensive conditioning.



#### 5.4.1 Input circuit monitor

#### Thermocouples

The input circuit monitor provides thermocouple checking for break and wrong polarity. An error is found, if the value of the measured thermovoltage is by more than 30 K below the span start.

Pt100 measurements and potentiometric transducers are monitored for break and short circuit.

#### **Current and voltage signals**

With current (0/4...20 mA) and voltage signals (0/2...10V), monitoring for exceeded range (I > 21.5 mA or U > 10.75 V) and for short circuit (I < 2 mA or U < 1 V) with "life zero" signals is provided.

Sensor errors can be output as control signal. In case of error, upscale or downscale action of the input ciruits are possible.

Moreover, a "substitute" value can be defined with controller KS94.  $(\mathbf{f})$ 

Unless the main correcting variable, but e.g. external set-point, set-point offset or external output limiting are concerned, control can be continued also with failure of an auxiliary variable. After removal of a sensor error, the controller waits, until the input signal has settled (approx.10s), before the controller is initialized (outputs switched off during several seconds).

#### 5.4.2 Scaling

Standard signals mA and V are scaled according to the physicl measuring range of the transformer (x0, x100).

With potentiometric transducer measurements (INP1, INP6), "calibration" is according to a well-proven, practice-oriented method. Bring the transducer to span start and then to span end position and "calibrate" it for 0% or for 100% by pressing a key at parameter level. Calibration is basically a scaling procedure, whereby gradient and zero correction are calculated automatically via the firmware.

#### 5.4.3 Linearization

Generally, thermocouples and Pt100 are measured in the overall physical measuring range according to data sheet, and linearized according to the relevant allocation table. Linearization is realized by error curve approximation with up to 28 segment points.

#### 5.4.4 Additional measurements

Dependent of configured sensor type, additional and corrective measurements are required. The amplifier zero is checked with all measurement types and taken into account during measurement value calculation. The lead resistances with Pt100 and potentiometric transducer, and the cold-junction reference temperature (internal TC) with thermocouples are measured additionally.

#### 5.4.5 Filter

In addition to filtering in the analog section of each input signal, a 1st order filter is adjustable (filter time constant 0,5...9999s; configuration).

#### 5.4.6 Scanning intervals

The internal scanning interval of controllers KS92 and KS94 is 100ms.

A survey of input and output scanning intervals, front LEDs, operating keys and serial interfaces is given in the following table.

Description	Scanning interval	Circuit board
Serial interfaces	100 ms	B, front
LEDs	100 ms	front
Keys	100 ms	front
INP1	200 ms	А
TC, with thermocouples	2,4 s	А
Compensation measurement of the lead resistance with Pt100 and transducer	2,4 s	А
Zero correction using an internal reference voltage	2,4 s	А
INP3	200 ms	С
INP4	200 ms	С
INP5	800 ms	А
INP6	400 ms	Α
OUT 1,2,4,5	100 ms	Р
OUT3	100 ms	С
di37	100 ms	В
di812	100 ms	С
do14	100 ms	В
do5,6	100 ms	С

#### 5.4.7 Linearization error

Thermocouples and Pt100 are linearized within nearly the overall physical measuring range. Linearization is with up to 28 segments, which are placed in the error curve optimally to compensate the linearity errors. As the error curve approximation is only by polygons and not by an nth order polynomial, the remaining error is zero in some points of the characteristic curve. Between these "zero points", however, there is a very low, though measurable remaining error. For reproducibility, however, this error is not relevant, because it would be reproduced in exactly the same point, if the measurement would be repeated under identical conditions.

#### 5.4.8 Temperature compensation

Measurement of the cold-junction reference temperature with thermocouples is using a PTC resistor. The temperature error thus determined is converted into mV of the relevant thermocouple type, linearized and added to the measurement value as correcting value with correct polarity. The remaining error with varying cold-junction reference temperature is approx. 0.5K/10K, i.e. about one twentieth of the error which would occur without compensation. Better results are possible with a controlled, external TC, which is adjustable within -99...+100°C dependent of temperature adjusted at the cold-junction reference.

With comparative measurements for assessment of the "reproducibility", however, constant environmental conditions are indispensable when working with internal TC! A draft at the PTC resistor of the cold-junction reference can be sufficient to produce a measurement error.

#### 5.4.9 Measurement value correction (optional)

The measurement value correction can be used for correcting the measurement.

**Prerequisite:** Configuration word **5.205**; XKorr = 1 ( $\rightarrow$  page 104)

In most case, the relative accuracy and reproducibility rather than the absolute one is of interest, e.g.

- measurement error compensation in a working point (set-point control)
- minimization of linerarity errors in a limited working range (variable set-point)
- conformity with other measuring equipment (recorders, indicators, PLCs, ...)
- compensation of the sensor, transmitter, etc. stray errors

The optional measurement value correction can be designed both for zero correction and gain matching. It corresponds to a scaling mx+b, with the difference that the controller firmware calculates the gain m and the zero offset b from the pre-defined values for process value (x1in; x2in) and set-point (x1out; x2out) of two reference points.

#### Example 1:

Zero offset			
x1in	$= 100^{\circ}C$	x1out	$= 100^{\circ}C + 1,5^{\circ}C$
x2in	= 300°C	x2out	$= 300^{\circ}C + 1,5^{\circ}C$

The difference between corrected values and input values is equal over the complete range.



Gain change (rotated around the coordinate origin)  $x1in = 0^{\circ}C$   $x1out = 0^{\circ}C$  $x2in = 300^{\circ}C$   $x2out = 300^{\circ}C + 1,5^{\circ}C$ 

The corrected values are equal to the input values at x1 in and x1 out, but the difference increases.



Zero and gain matching			
xlin	$= 100^{\circ}C$	xlout	= 100°C - 2,0°C
x2in	= 300°C	x2out	$= 300^{\circ}C + 1,5^{\circ}C$

The corrected values are already different at input values x1in and x1out and the difference increases additionally.



### 5.5 Signal pre-processing

Input value conditioning is followed by signal pre-processing.

The analog input signals can undergo further conditioning.

Func1 and Func2 are spacekeepers for configurable functions which can be selected from the following function library:



Each function can be used only once (either in Func1 or in Func2). The table gives a survey of inputs and usable functions.

Function	INP1 (C.220)	INP3 (C.320)	INP4 (C.370)	INP5 (C.420)	INP6 (C.470)
SCAL	Х	only with KS94	only with KS94	Х	Х
CHAR	Х		only with KS94		
SQRT	Х	only with KS94	only with KS94	Х	Х
LAG1	Х	only with KS94	only with KS94	Х	Х

SCAL - Scaling

Scaling is done according to equation  $OUT = m \cdot INP + b.$ Hereby, parameters m and b can be adjusted so that inverse characteristics can also be realized. Adjustable parameters: m = gain and b = offset

CHAR - Linearization Y Up to 8 adjustable segment points (value pairs xsi/ysi) can be used to simulate or linearize non-linear ys7 functions. The number of value pairs ys5 is limited to 8 (7 segments). If less than 8 value pairs are used, the first ys4 unused segment must be switched off by entry of the xs-value into "——". Offset and gradient for the ys1 relevant intervals are determined automatically from the adjusted value pairs. The segment points are interconnected by straight lines, so



that there is a defined output value (ys) for each input value (xs). Beyond the defined intervals, the first or last segment is prolonged. Adjustable parameters: for each input - (x1,y1), (x2,y2)...(x8,y8)

Note that the input values (x-values) must be entered in ascending order.

SQRT-	Square root The square root of the input signal is calculated and
	the result is multiplied by parameter "gain". OUT = gain * root INP
	If the value under the root is negative, the result is set to 0. Adjustable parameter: for each input - gain
- LAG1	Filter

G1 Filter The input value is taken to the output with delay. The delay is according to a 1st order e-function (1st order low pass) with the filter time adjustable with parameter Tf. Adjustable parameter: Tf = filter time



#### 5.6 Inputs



The input names and numbers were selected for utmost language-independent, international clarity of the inputs and outputs on the process value display (7 segments) during configuration. Digital inputs and output are marked with lower case letters to permit clear distinction of "0" and "o" on the

Digital inputs and output are marked with lower case letters to permit clear distinction of "0" and "o" on the display.

#### **INPUT**: - analog inputs

The signal inputs for the previously selected controller configuration are determined in this main group. The signal inputs for the selected controller function are displayed in the configuration menu. As with control function configuration, a large number of applications can be covered by determination of the main configuration. Special cases can be matched and adjusted by additional option configuration at the second level. INP2 is not available with controllers KS92/42. Therefore, there is a gap in the input sequence. Max. the following five signal inputs are available:

- process value x: INP1, INP3 or INP4
- external set-point We, dWe: INP5
- position feedback yp: INP6

#### 5.6.1 Signal input 1 INP1 (main variable x1) ( $\rightarrow$ $\complement$ $\circlearrowright$ $\circlearrowright$

The analog input INP1 is used as main variable x1.

The input sensor type can be determined as thermocouple, resistance thermometer, potentiometric transducer or as a standard signal. The physical unit is freely selectable. If required, additional input configurations can be determined with the extra configuration.



#### **Thermocouple input**

The following thermocouple types are configurable as standard:

Type E, J, K, L, N, R, S, T and W to IEC584.

The signal behaviour can be affected by configuration of the following points. Distinction of internal and external temperature compensation is made ( $\rightarrow$  £.205).

- Internal temperature compensation: The compensating lead must be taken up to the controller terminals. Lead resistance adjustment is not required.
- External temperature compensation: A separate cold-junction reference with a fixed reference temperature must be used (configurable between 0 and 100°C) (→ £.2 10) The compensating lead must be taken only up to the cold-junction reference, from which point

copper lead must be used. Lead resistance adjustment is not necessary.

- Upscale (set-point << process value) or downscale (set-point >> process value) action of the built-in TC monitoring can be configured, or a fixed substitute value can be used for the action. ( $\rightarrow$  L.205).
- For input value processing, a filter time constant with a numeric value between 0,5 and 999,9 is adjustable ( $\rightarrow$  **L2** 14).
- A process value correction is configurable ( $\rightarrow$  **L205**).

The order of configuration is as follows:  $1.200 \rightarrow 1.205 - (1.210) - (1.214)$
# **Resistance thermometer input**

Resistance thermometer, temperature difference

With a resistance thermometer, the signal behaviour with sensor break can be determined  $(\rightarrow L.205)$ . Temperature compensation is not required and therefore switched off. With temperature difference measurement, calibration by means of short-circuit is required.

Lead resistance adjustment can be done using e.g. the 10 calibrating resistor (order no. 9404 209 10101). Dependent of sensor type, the controller must be configured for one of the following inputs:

- resistance thermometer Pt 100 with linearization
- temperature difference with 2 x Pt 100 and linearization
- linear potentiometric transducers

For input value processing, a filter time constant with a numeric value within 0,5 and 999,9 is adjustable  $(\rightarrow L.2 14)$ . The decimal point (digits behind the decimal point) and process value correction can be configured  $(\rightarrow L.205)$ .

Configuration is in the following order:  $L200 \rightarrow L205 - (L214) - (L215)$ 

#### **Resistance thermometer Pt 100**

The two ranges -99,9...+250,0 °C and -99,9...+850,0 °C are configurable ( $\rightarrow$  **L205**). Connection is possible in two or three-wire circuit. Measuring leads must be of copper. The input circuit monitor responds with -130°C (sensor break or lead break). The output action is configurable for:

- upscale (set-point << process value) ( $\rightarrow$  £.205)
- downscale (set-point >> process value) ( $\rightarrow$  **[.205**)
- a fixed value (in case of error, the selected number is used for the value to be measured ( $\rightarrow$  L2 (3).

## Resistance thermometer in 2-wire connection:

For lead resistance adjustment, disconnect the measuring leads from the controller and short-circuit them in the connecting head of the resistance thermometer. Now, measure the resistance of the measuring lead using a resistance bridge and connect a calibrating resistor ( $R_a$ ) of the same value.





12

13

14

15

#### **Resistance thermometer in 3-wire connection:**

The resistance of each input lead must not exceed 30  $\Omega$ . Lead resistance adjustment is not necessary, provided that the resistances Ra of the input leads are equal. If necessary, they must be equalized using a calibrating resistor.





#### Temperature difference 2 x Pt100

Range  $\vartheta_1 \cdot \vartheta_2$  is within -200,0...+300,0 °C ( $\vartheta_2$  = referene). For lead resistance adjustment for INP1, take the controller into manual operation and select calibrating parameter × $\vartheta c$  as shown in Fig.:12. Press the selector key to prepare the calibration ("c" in the display × $\vartheta c$  flashes). Now, short circuit the input leads at the two PT100 resistors. Press the selector key again to store the measured resistance value as lead resistance, in order to correct the subsequent measurements accordingly. Remove the short circuits of the leads.



#### **D** Potentiometric transducer

The overall resistance  $\leq 500 \Omega$  incl. 2 • RL. Calibration or scaling are done with the sensor connected. An input circuit monitor can be configured for sensor or lead break or short circuit. The action, process value correction and decimal point are adjustable ( $\rightarrow$  £.205 and £.2 13). Configuration is in the following order: £.200 $\rightarrow$  £.205 - £.2 11 - £.2 12 - £.2 14

Calibration for  $X_0$  and  $X_{100}$  is at parameter level as follows.

Calibration is only possible with the controller set to manual mode. Potentiometric transducer calibration for  $X_0$  or  $X_{100}$  is possible via the interface and the front foil. Calibration is in two steps:

Fig.: 12 Selecting parameter ×0c /×100c



• Calibration for X<sub>0</sub>:

Select  $\times \Theta \subset$  as shown in Fig.: 12. Press the selector key, the " $\subset$ " on the display  $\times \Theta \subset$  starts blinking. Now, bring the potentiometric transducer into the position for X<sub>0</sub> (usually lower end position). The instantaneously valid value for INP1 appears on display 1. Press the selector key again to store this actual value as X0.

Calibration for X<sub>100</sub> must be done accordingly.
 Select ×100c. Press the selector key. The "c" of the display ×100c starts blinking. Now, bring the transducer into the position for X<sub>100</sub> (usually upper end position). The instantaneously valid value for INP1 is shown on display 1. Press the selector key again to store this actual value as X<sub>100</sub>.

#### Standard 0/4...20 mA signal input

#### The input resistance is 50 $\Omega$

During configuration, distinction of 0...20 mA and 4...20 mA is made. For the 4 ... 20 mA standard signal, the behaviour with sensor break can be determined ([.2, 1]). M<%-2>oreover, the decimal point and thus the digits behind the decimal point are configurable ( $\rightarrow$  [.200]). Additionally, a physical input signal scaling by means of X<sub>0</sub> and X<sub>100</sub> is possible ( $\rightarrow$  [.200] and [.202]). For input value processing, a filter time constant with a numeric value within 0,5 and 999,9 is adjustable ( $\rightarrow$  [.2,14]). For configuration, proceed in the following order:  $[.200] \rightarrow [.200] + [.200] - [.200$ 

12

13

14

15

16

mΔ

#### **0/2...10** V input

The input resistance is  $\geq 100 \text{ k}\Omega$ 

During configuration, distinction of 0...10 V and 2...10 V is made. For the 2 ... 10 V standard signal, the output action with sensor break can be determined ( $[.2 \ 13]$ ). Moreover, the decimal point and thus the digits behind the decimal point are adjustable ( $\rightarrow$  [.200]). Additionally, a physical input signal scaling by means of X<sub>0</sub> and X<sub>100</sub> is possible ( $\rightarrow$  [.200] 1 and [.2002]). For input value processing, a filter time constant with a numeric value within 0,5 and 999,9 can be used ( $\rightarrow$  [.214]). For configuration, proceed in the following order:  $[.200] \rightarrow [.200] + [.2002] + [.2005]$ 

# 5.6.2 Additional signal input 3 / INP3 (optional) ( $\rightarrow E.BBB$ )

This signal input is only available with option p.c.b "C" fitted.

It may be configured for ratio variable  $x_2$  or disturbance variable  $z (\rightarrow L, 105 \text{ or } L, 100)$ .

Selection of standard input signals 0...20 mA and 4...20 mA is possible. The physical unit can be configured. The input resistance is 50  $\Omega$ . For the 4...20 mA standard signal, the output action with sensor break can be configured ( $\rightarrow \xi.305$  and  $\xi.313$ ).

Physical input scaling is possible by determination of 0 % and 100 % ( $\rightarrow$ E.30 1 and E.302). Moreover, the decimal point, i.e. the digits behind the decimal point can be configured ( $\rightarrow$ E.300).

For input value processing, a filter time constant with a numeric value within 0,5 and 999,9 is adjustable ( $\rightarrow$  **L.3** 14)

For configuration, proceed in the following order:  $L:300 \rightarrow L:301 + L:302 + L:305 + L:313 + (L:313)$ 

# 5.6.3 Additional signal input 4 / INP4 (optional) ( $\rightarrow 1.350$ )

This signal input is only available with option p.c.b. "C" fitted.

It can be configured for three-element control  $x_3$ , external set-point or external set-point offset ( $\rightarrow L$ . [80]). Selection of 0...20 mA and 4...20 mA standard input signals is possible. The physical unit can be configured. The input resistance is 50  $\Omega$ . For the 4...20 mA standard signal, the output action with sensor break can be determined ( $\rightarrow L.355$  and L.353).

A physical input scaling is possible by determination of 0 % and 100 % ( $\rightarrow$ E.35 / and E.352). Moreover, the decimal point, i.e. the digits behind the decimal point can be configured ( $\rightarrow$ E.350).

For input value processing, a filter time constant with a numeric value within 0,5 and 999,9 can be adjusted  $(\rightarrow \textbf{L}, \textbf{354})$ .

For configuration, proceed in the following order:  $L.350 \rightarrow L.351 - L.352 - L.355 - L.353 - (L.354)$ 

# 5.6.4 Signal input 5 / INP5 (ratio variable x2, ext. set-point Wext) ( $\rightarrow$ [.400)

Analog input INP5 is used for connection of the signal for ratio variable x2 or for the external set-point Wext, if option p.c.b. is not fitted in the controller and with the function selected during controller configuration. Selection of 0/4...20 mA and 0/2...10 V signals is possible. The physical unit can be configured.

This input is a difference input. Terminal A9 is used as reference potential (Common). With voltage signals, terminal A6 must always be connected with terminal A9.

The input resistance is 50  $\Omega$  as mA input and  $\geq$  100 k $\Omega$  as V input.

For the 2 ... 10 V or 4...20 mA standard signals, the output action with sensor break can be determined ( $\rightarrow$  **L.405** and **L.413**). Moreover, the decimal point, i.e. the digits behind the decimal point can be selected (**L.400**). Additionally, a physical input scaling by determination of 0 % and 100 % is possible ( $\rightarrow$  **L.401** and **L.402**).

For input value processing, a filter time constant with a numeric value within 0,5 and 999,9 can be adjusted  $(\rightarrow \Sigma, \Upsilon, \Upsilon)$ 

Configuration is in the following order:

C.400→E.401-E.402-E.405-E.413-(E.414)

See also external set-point Wext page 45 and ratio controller page 49

### 5.6.5 Signal input 6 / INP6 (auxiliary variable yp, position feedback yp) ( $\rightarrow$ L450)

The signal for auxiliary variable vp or position feedback is configured at analog input INP6, if this was selected during controller configuration.

For this input, the decimal point and thus the digits behind the decimal point can be selected ( $\rightarrow \xi.450$ ) Moreover, a physical input signal scaling by determination of 0% and 100 % is possible ( $\rightarrow$  £.45 L and [.452).

The output action with sensor break can be selected only with 4...20 mA standard signal ( $\rightarrow$  £.455 and E.463).

For input value processing, a filter time constant with a numeric value within 0,5 and 999,9 can be adjusted  $(\rightarrow$  **E.454**).

Configuration is in the following order:  $(.450 \rightarrow (.451 - (.452 - (.455 - (.463 - (.464$ 

See also position feedback yp page 56

#### 5.6.6 Digital inputs "di"

Energization of digital inputs "di" via an external 24 V DC supply is required. The current consumption for each input is 5 mA.

The digital inputs can be energized by one or several voltage sources (e.g. 24V PLC control outputs). Note that the negative potentials of the voltage sources are identical and must be taken to the corresponding controller connecting terminals.

#### **Connecting examples:**



#### Digital inputs di1 and di2

Dependent of configuration (L, 190 and L, 191), digital inputs d1 and d2 can control the following operations. Allocating several functions to a digital input is also possible.

- Switch-over between internal set-point W (0) and second set-point W2 (1)
- Switch-over between automatic (0) and manual (1) mode
- Set-point offset switch-on; normal (0) offset (1)
- Switch-over between normal correcting value (0) and safe correcting value (1)
- Switches the controller ON(0) or OFF(1)
- Switch-over between PI (0) and P (1) with 2/3-point and continuous controllers or feedback switch-off with 3-point stepping controllers
- Bumpless switch-over between normal correcting value (0) and safe correcting value (1)
- Bumpless switch-over to the internal set-point (tracking only di2) OFF (0) ON (1)

#### Digital inputs di3 to di12

di3	used for switch-over between local (0) and remote (1).									
di4	used for sw	used for switch-over between program STOP (0) and START (1) ( [. 192; SPrSt.).								
di5	used for pro	used for programmer RESET; normal (0), reset (1).								
di6/di7	used for pro	ogram	numbe	er sele	ction with program	mer.				
	-	-								
T	di6	0	1	х		di8	0	1	0	1
	di7	0	0	1		di9	0	0	1	1
	Program	1	2	3		Parameter set	0	1	2	3

di7/di8 used for program number selection with programmer.

- di10 minimum delimitation of the correcting variable with 3-pnt.stepping controller di11 maximum delimitation of the correcting variable with 3-pnt.stepping controller and can be configured for switching on the effective set-point offset (£.190:5dWorn).
- di12 switches over bumplessly to the internal set-point (tracking) OFF (0) ON (1). and can be used for switching over to the second set-point W2 (**L ! 90**) OFF (0) ON (1).

# 5.7 Outputs

The input names and numbers were selected for utmost language-independent, international clarity of the inputs and outputs on the process value display (7 segments) during configuration. Digital inputs and output are marked with lower case letters to permit clear distinction of "0" and "o" on the display.

#### **OUT: outputs**

Dependent of hardware, there may be four switching outputs or three switching and one analog output. Additionally, there may be optional output OUT3, which is located on plug-in options p.c.b. "C". OUT1 can be ordered as switching or continuous output. Outputs OUT2, OUT4 and OUT5 are always switching and output OUT3 is always analog.



Behaviour of outputs with initialisation

All outputs are switched off for 100 ms at the end of initialisation. Analog outputs take over the lower output value (0/4 mA) .

# 5.7.1 Signal output 1 OUT1 $(\rightarrow \complement.5 \square \square)$

Signal output OUT1 is used for controller correcting variable Y1/Y2. As it is a universal output, extensive functions can be configured.

Which signal shall be taken to this output must be determined at configuration word [.500; Src :

• 00: none (output switched off)	• 05: control deviation xw	• 20: Wint	• 25: Alarm 1 (Limit 1)
• 01: controller output Y1/Yout1	<ul> <li>10: process value xeff</li> </ul>	• 21: Wext	• 26: Alarm 2 (Limit 2)
• 02: controller output Y2/Yout2	<ul> <li>11: process value x1</li> </ul>	• 22: dWext	• 27: Alarm 3 (Limit 3)
• 03: controller output Ypid	<ul> <li>12: process value x2</li> </ul>	• 23: Weff	• 28: Alarm 4 (Limit 4)
• 04: position feedback Yp	• 13: process value x3	• 24: Wp (programmer)	

With a controller with continuous output, the output signal type can also be determined. 0...20 mA, 4...20 mA or logic signal 0 and 20 mA can be selected.

Direct or inverse motor actuator output action can be adjusted.

# 5.7.2 Signal output 2 OUT2 ( $\rightarrow$ [.530)

Switching signal output OUT2 is used for controller correcting variable Y1/Y2. This is a relay output. Which signal should be taken to this output must be determined at configuration level. Selection of controller output Y1/2 and alarm signals (limit) is possible. Direct or inverse motor actuator output action.

# 5.7.3 Additional signal output 3 OUT3 (optional) ( $\rightarrow$ L.550)

This output is only provided in conjunction with options p.c.b. "C". Analog signal output OUT3 is used for a selectable controller signal. As this is a universal output, it can be configured for extensive functions.

Which signal shall be taken to this output must be determined at configuration level (1.550). Selection between various controller outputs, process values and set-points is possible. Direct or inverse motor actuator action is selectable. The output signal type can be determined. Selectable are 0...20 mA, 4...20 mA or logic signal 0 and 20 mA.

Before the signals reach output OUT3, they can be processed again by means of function block "Func" ( $\rightarrow$  **L.555**). Configuration parameter Func permits selection of direct signal output, scaling and linearization.

20 m/

With direct signal output, the subsequently adjustable parameters  $X_0$  and  $X_{100}$  are not taken into account (E.5 70 and E.5 7 1)

#### **Scaling**

Scaling is adjustable according to reference values  $X_0$  and  $X_{100}^{\cdot}$ 

Example 1:

This scaling is a simple allocation of 0...100 to 0...20 mA. The output is determined for 0...20 mA.  $X_0 = 0$   $X_{100} = 100$ When applying value 50, the output is 10 mA.

#### Example 2:

This scaling is an allocation of 0...200 to 0...20 mA. The output is determined for 0...20 mA.  $X_0 = 0$   $X_{100} = 200$ When applying value 50, the output is 5 mA.

#### Example 3:

This scaling is an allocation of 10...110 to 0...20 mA, whereby an offset is provided. The output is determined for 0...20 mA.  $X_0 = 10$   $X_{100} = 110$ When applying value 50, the output is 8 mA.

#### **CHAR** - Linearization

8 adjustable segment points (value pairs xsi/ysi) can be used for simulation Y or linearization of non-linear functions. ys8 The number of value pairs is limited to 8 (7 ys7 ys6 ys5 segments). When using less than 8 value pairs, the first unused segment must be switched off by entry of the xs value into"----". ys4 Offset and gradient for the relevant intervals ys3 ys2 are calculated automatically from the adjusted value pairs. ys The segment points are interconnected by

straight lines so that each input value (xs) corresponds to a defined output value (ys). Beyond the defined segments the first or the



last segment is prolonged. Adjustable parameters: (x1,y1), (x2,y2)...(x8,y8)

Input values (x-values) have to be set in ascending order.

# 5.7.4 Signal output 4 OUT4 ( $\rightarrow$ $\complement$ 5 $\Im$ $\square$ )

Switching signal output OUT4 can be used for various signals. This is a relay output. Which signal shall be taken to this output must be determined at configuration level. Selection of controller output Y1/2 and alarm signals (limit) is possible. One of the four programmer outputs 1...4 and programmer end is possible.

Direct or inverse motor actuator output action can be adjusted.

## 5.7.5 Signal output 5 OUT5 ( $\rightarrow$ [.59])

Switching signal output OUT5 can be used for various signals. This is a relay output.

Which signal shall be taken to this output must be determined at configuration level. Selection of controller output Y1/2 and alarm signals (limit) is possible. One of the four programmer outputs 1...4 and programmer end is possible.

Direct or inverse motor actuator output action can be adjusted.

#### 5.7.6 Digital outputs do1 to do6

do1	indicates the status of control output 1 with programmer.
do2	indicates the status of control output 2 with programmer.
do3	indicates the status of control output 3 with programmer.
do4	indicates the status of control output 4 with programmer.
do5	indicates, if the controller is in manual or automatic mode, or
	the y1 condition with switching controllers ( <b>[.596</b> ).
d06	indicates, if the controller uses the external or the internal set-point, or
	status v2 with switching controllers $(5.537)$ .

#### 5.7.7 Input and output survey

allocation of analog inputs / outputs and circuit boards

·	<u>circ</u> u	<u>iit board</u>		circuit board			
process inputs	A	C (option)	process outputs	Р	C (option)		
INP1	×		OUT1	×			
INP3		×	OUT2	×			
INP4		×	OUT3		×		
INP5	×		OUT4	×			
INP6	×		OUT5	×			

allocation of digital inputs / outputs and circuit boards

	L	circuit board	
control inputs	Α	B (option)	C (option)
di1	×		
di2	×		
di3		×	
di4		×	
di5		×	
di6		×	
di7		×	
di8			×
di9			×
di10			×
di11			×
di12			×

control outputs	circuit_board							
control outputs	B (option)	C (option)						
do1	×							
do2	×							
do3	×							
do4	×							
do5		×						
do6		×						

	X1	X2	X3	Ext. set-point	Ext. set-point offset	Auxiliary variable z	Position feedback	OVC	Min/Max selection
INP1	X								
INP3		X				×			×
INP4			X	×	×	×		X	
INP5		X		×	×				
INP6				×	×	×	×		

Function allocation of analog inputs

Function allocation of control inputs

Functions	di1	di2	di3	di4	di5	di6	di7	di8	di9	di10	di11	di12
Wint / Wext	X	X										
Tracking on / off		X										X
$\Delta \mathbf{W}$ on / off	X	X									X	
w / W2	X	X										X
Auto / Man	X	X										
PI / P	X	X										
Y / Y2	X	X										
Controller on / off	X	X										
Programmer Run / Stop				X								
Programmer Reset					X							
Selection of programs						X	X					
Remote / Local			X									
Parameterset								X	×			
OVC+ (Three-point stepping controller)										X		
OVC- (Three-point stepping											×	
disabling <sup>1)</sup>	×	X										
OVC off/on	I									X		

Function allocation of outputs

Functions	OUT1	OUT2	OUT3	OUT4	OUT5	do1	do2	do3	do4	do5	do6
Controller output 1	X	X	X	X	X					X	
Controller output2	X	X	×	X	×						X
Alarm 1	X	×		×	×						
Alarm 2	X	×		×	×						
Alarm 3	X	X		×	×						
Alarm 4	X	X		×	×						
Process values (x1, x2, x3, x <sub>eff</sub> )	X		X								
Set-points (w, weff, wext, dwext, wp	X		×								
Control deviation (xw)	X		×								
Correcting variable Y <sub>pid</sub>	X		X								
Position feedback (Yp)	X		×								
Contr. outputs 1				X	×	X					
Contr. outputs 2				X	×		X				
Contr. outputs 3				×	×			X			
Contr. outputs 4				×	×				X		
Program end				×	×						
Status auto/man										X	
Status Wint/Wext											X

<sup>1)</sup> auto/manual key disabling, set-point adjustment, controller switch-off, value adjustment and programmable controller operation.

# 6 Set-point functions

# 6.1 Terminology

W	internal set-point	
we	external set-point	
wp	programmer set-point	
W2	second (internal) set-point	
Weff	effective set-point	
SWi/e	signal source for "internal/external" set-point switch-over	C. 190
Sw/W2	signal source for "weff / W2" set-point switch-over	E. (90
SWdon	set-point offset switch-on	E. (90
S Wd	signal source for set-point offset	C. 180
W d	set-point offset type	C. 106
SWext	signal source for external set-point	C. 180
WTrac	tracking function switch-on	C. 106
STrac	signal source for tracking	C. 190
WSel	automatically selected lowest or highest set-point	E. 106

#### 6.2 General

The following set-point functions are selectable during configuration C.100 using parameter WFunc.

In addition to the described effective set-points, switching over to the second set-point W2 is possible.

Switch-over is via signal source Sw/W2 determined in configuration parameter C.190.

i

#### **Set-point** (WFunc = 0)

With set-point control, the set-point is determined by internal set-point W<sup>-</sup>



INP 5/6/4

INP 1

х

w

┛

Ĺ.,

-- **C** e/i W2

**A** w/W2 Weff

> w X

#### **Set-point/cascade** (WFunc = 1)

we With set-point/cascade control, switching over between internal set-point W and external set-point We is possible. Switching over is done via signal source  $\Im \mathbb{U} i \neq \mathbb{U}$  determined in configuration parameter E. 190.



#### **Programmer** (WFunc = 2)

With programmer control, the set-point is determined by the internal programmer Wp. Switching over to the internal set-point W is possible and must be done via the signal source SWi/e determined in configuration parameter [. 190.

#### **Set-point with external offset** (WFunc = 3)

With set-point control with external offset, the effective set-point is determined by internal set-point W, however, it can be affected by external offset dW. The type of offset (additive or factor) is determined during configuration **[.**  $\square$  **b** by parameter  $\square$  **W**. The offset is switched on via signal source Suldon determined in configuration parameter [. 190.



**Set-point/cascade with internal offset** (WFunc = 4)

With set-point/cascade control with internal offset, switching over between internal set-point W and external set-point We is possible. Switching over is done via signal source  $\exists Wi \neq e$  determined in configuration parameter [.190.

External set-point **We** can be affected by an internal offset **dW**. The offset type (additive or factor) is determined during configuration

[.105] by parameter dW. The offset is switched on via signal source SWdon determined in configuration parameter [.190].

#### Set-point/cascade with external offset (WFunc = 5)

Set-point/cascade with external offset permits switch-over between internal set-point **W** and external set-point **We**. Switch-over is via signal source  $\exists Ui \neq e$  determined in configuration parameter **L**.  $\exists II$ . External set-point **We** can be affected by an external offset **dWe**. The offset type (additive or factor) is determined during configuration

[. 105 by parameter dW. The offset is switched on via signal source SWdon determined in configuration parameter [. 190.

#### **Programmer with internal offset** (WFunc = 6)

With program control with internal offset, the set-point is determined by internal programmer **Wp**.

The programmer value can be affected by an internal offset **dW**. The set-point offset type (additive or factor) is determined during configuration  $\int dP_{\rm c}$  by parameter **d**||. The effect is grait hed on via

configuration [.105] by parameter dW. The offset is switched on via signal source SWdon determined in configuration parameter [.190]. The resulting set-point or internal

signal source  $\exists w \exists \exists n$  determined in configuration parameter L,  $\forall \exists u$ . The resulting scepoint of methods set-point W can be selected. Switching over is done via signal source  $\exists W \mathbf{i} \neq \mathbf{e}$  determined in configuration parameter L. **190**.

#### **Programmer with external offset** (WFunc = 7)

With program control with external offset, the set-point is determined by internal programmer **Wp**.

The programmer value can be affected by an external offset **dW**. The type of set-point offset (additive or factor) is determined during

configuration L. (DS by parameter dW. The offset is switched on via signal source SWdon determined in configuration parameter L. (BD. This set-point can also be affected by an external offset dWe. Switching over between the resulting set-point and internal set-point W is also possible and must be done via signal source  $SWi \neq e$  determined in configuration parameter L. (BD.









# 6.3 Detailed set-point function block diagrams

The following set-point function block diagrams illustrate the interactions of configuration parameters and possible control operations.











Fig.: 15 Set-point control with external offset [. 100; WFunc = 3







Fig.: 17 Programmer with ext. or int. offset [.100; WFunc = 5/7

### 6.4 Safe set-point W<sub>2</sub>

Second set-point W2 can always be activated with highest priority.

In the past, W2 was called "safe set-point". Whether W2 can have safety functions, or whether it is only a pre-defined start position in defined process conditions is determined only by the way it is used and integrated into an automation concept.

Dependent of configuration, switch-over to set-point W2 is possible via interface, front operation, timer or one of control inputs di1,di2 or di12 ( $\rightarrow$ L. 191).

Second set-point W2 is handled with priority. If W2 was selected anywhere (front panel, interface or the relevant control input), switching over at another facility is not possible.

# 6.5 External set-point Wext

Dependent of configuration, switching over between internal and external set-point via interface, front panel operation or one of control inputs di1 or di2 is possible ( $\rightarrow L$ . [3]). For making the external set-point effective, a 1 signal (24 V) must be connected on the int/ext contact. For activating the internal set-point, a 0 signal (0V) must be applied to the int/ext contact.

Analog input "Wext" is connected to INP5, however, it can be configured also for INP4 (galvanically isolated) or INP6 ( $y_P$  input)( $\rightarrow L$ . 181), if necessary. Signal pre-processing (Func1, Func2) permits adjustment of the required set-point or correction characteristic as a function of the input signal. (dependent of configuration:  $\rightarrow$ INP5 L.3 10, INP4 L.4 20 or INP6 L.4 10).



Internal set-point W has priority. If the internal set-point was selected anywhere (front panel, interface or the relevant control input), switching over to external set-point We at another facility is not possible.

# 6.6 Set-point offset

The Set-point offset (internal dW or external dWe) can be added to the effective set-point or multiplied by it  $(\rightarrow L, III5; dW)$ . Examples for an additive set-point offset are "reduced stand-by set-point" and "outside temperature-dependent supply temperature control". Set-point offset as a factor can be used e.g. for split load or O2 correction.

Dependent of configuration, the set-point offset can be triggered via interface, front panel operation, or via one of control inputs di1,di2 or di11( $\rightarrow$  L. 190; SdWon). For activating the set-point offset, a 1 signal (24 V) must be connected to the relevant contact.

For de-activating the set-point offset, a 0 signal (0V) must be applied to the contact. Analog input "S Wd" is connected to INP5, however, it can be configured also for INP4 (galvanically isolated) or INP6 (yP input) ( $\rightarrow L$  180; 5dW), if necessary. Signal pre-processing (Func1, Func2) permits adjustment of the required set-point or correction characteristic as function of the input signal. (dependent of configuration:  $\rightarrow$  INP5 L310, INP4 L420 or INP6 L410)



"Offset activated" has priority. With selection "offset active" at anywhere (front panel, interface or the relevant control input), switching over at another facility is not possible.

# 6.7 Bumplessness

#### 6.7.1 Set-point change

Set-point change in both direction is always bumpless. The effective set-point Weff approaches the modified set-point (target) linearly, whereby gradients **Grw+** and **Grw-** adjustable at parameter level determine the slope. The gradient function is also active with programmer, however, it is not effective as long as the program profile causes slower set-point changes than the adjusted gradients. Hereby, the gradient setting can be used as safety function with incorrectly adjusted programmer.

For second set-point W2, an independent gradient **Grw2** which is valid for the two switch-over directions was introduced.

The gradient function is switched off with Grw+ and Grw- or Grw2 set to "----".



Fig.: 18 Ramp function with set-point change

## 6.7.2 Set-point switch-over (w/w2, Wext/Wint, w/wp, Controller 'On')

Control with the new set-point starts linearly from the instantaneous process value. The slope of the ramp is determined dependent of direction by Grw+, Grw- or Grw2. This is also valid, if the process value at switch-over time is out of the adjustable set-point range W0/W100 (e.g. during start-up).

In this case, controller 'On' means controller power supply switch-on. For activating the gradient with controller signal '5Coff = On GrwOn must be used ( $\rightarrow$  see also page 59).



Fig.: 19 Ramp function with set-point change

# 6.8 Tracking

# 6.8.1 Set-point tracking ( $\rightarrow$ [.] [] 5)

When switching over between the various set-points (We and WP), undesirable set-point steps may occur. These steps can be attenuated using the set-point tracking function.

With set-point tracking, the we/wp used so far is stored as internal set-point 'w' when switching over from we or wp  $\rightarrow$  w. When switching back (w  $\rightarrow$  we or wp), start-up is dependent of Grw+/- we or wp setting (see  $\rightarrow$  Fig.: 20).

The actual controller behaviour, process value or set-point tracking, is determined in configuration code L. 105; WTrac.

Dependent of configuration, this setting can be triggered via interface, front-panel operation or one of control inputs di2 or di12 ( $\rightarrow L$  **19** ). However, only the switch-over type is prepared at this faciliy, without selecting between internal and external set-point.

For preparing the bumpless switch-over, a 1 signal (24 V) must be connected to the external contact. For direct switch-over, a 0 signal (0 V) must be applied to the contact.

Bumpless switch-over has priority. With bumpless switch-over selected anywhere (front-panel, interface or relevant control input), switch-over at another facility is not possible.



Fig.: 20 Set-point tracking with switch-over to internel setpoint

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# 6.8.2 Process value tracking

The set-point may be far away from the instantaneous process value (e.g. during start-up). In this case, the process value tracking function can be used for attenuation of the step which may occur. Process value tracking causes storage of the process value as set-point, whereafter line-out to the actually required set-point is done slowly according to parameters Grw+/-.

Whether process value or set-point tracking is required is determined in configuration code C.106 - WTrac. Dependent of configuration, this setting can be made via interface, front panel operation or one of control inputs di2 or di12 ( $\rightarrow$  L.19D).

However, the type of switch-over is only prepared at this facility, without actually selecting between external and internal set-point.

For preparing bumpless switch-over, a 1 signal (24 V) must be connected to the relevant contact. For direct switch-over, a 0 signal (0V) must be applied to the contact.

Bumpless switch-over has priority. With bumpless switch-over selected anywhere (front panel, interface or relevant control input), switching over at another facility is not possible.



Fig.: 21 Process value tracking with switch-over to internal set-point W

#### 6.8.3 MIN/MAX selection WSel

Dependent of set-point WSel configuration, effective set-point Weff can be prevented from being below or above the value determined by analog input INP3 ( $\rightarrow L$ . 105).

This function can be used, for instance, during combustion control, whereby excess air is indispensable (crosswise interlocking of air and fuel supply).

The min/max selection can be activated also with set-point functions varying from those shown below.

Fig.: 22 Min/Max selection with internal offset Fig.: 23 Min/Max selection with external offset



# 7 Process value calculation

Fig.: 24 Standard conroller

# 7.1 Standard controller

The process variable measured via analog input INP1 and processed, if necessary, using functions Func1 and Func2 is used as process value x by the controller.



# 7.2 Ratio controller

Process control frequently requires various components to be mixed into a product. These components must be mixed according to a given ratio. The main component is measured and used as reference for the other components. With increasing flow of the main component, the flow of the other components will increase accordingly. This means that process value x used by the controller is determined by the ratio of two input variables instead of being measured as one process variable.

For optimum combustion, the fuel-air ratio must be controlled. With stoichiometric combustion, the ratio is selected so that there are no residues in the waste gas. In this case, the relative instead of the physical ratio is displayed as process value and adjusted as set-point 1. If the transmitters used by the controller use a stoichiometric ratio, l = 1 is exactly met with restless combustion. With a process value display of 1,05, the instaneous air excess is clearly 5%.

The amount of air required for atomizing is taken into account by constant N0 (Para  $\rightarrow$  Input  $\rightarrow$  IstW  $\rightarrow$  NØ). For selecting a ratio controller, the [  $\xi$  YP = 1 in [. (DD must be entered. Moreover, configuration words [. (D] L[. (D] must be taken into account.

# 7.2.1 Conventional ratio control:

Calculation so far required scaling of the ratio variables for a range of 0...100 % (x0, x100).

If this method shall remain unchanged, factor "s" must remain unchanged with respect to factory setting "s =1". In this case, the control deviation is formed according to

relation

$$\mathbf{x}\mathbf{w} = (\mathbf{x}\mathbf{1} + \mathbf{N}\mathbf{0}) - \lambda \bullet \mathbf{x}\mathbf{2}$$

In this case, the physical (%) and the relative ratio are identical so that the displayed process value  $x_1/x_2$  also corresponds to the relative ratio. Everything is as usual. The individual flow rates can be displayed with unit "%" at the extended configuration level.

# 7.2.2 Additional possibilities of ratio control with KS92/94

The two requirements, i.e. control of the relative ratio and

display of the material flow rates in physical units are met by means of the material-specific (stoichiometric) factor "s". For display of the individual material flow rates in physical units (e.g. Nm<sup>3</sup>/h) at the extended operating and display level, the two flow rates available as mA signals are scaled in physical units, i.e. they can also be displayed directly, e.g. in Nm<sup>3</sup>/h. Set-point W<sub>eff</sub> effective as a relative ratio is multiplied by the stoichiometric factor (e.g. s = 10). This means that "stoichiometric" material flow rates can be used for calculating the control deviation. The instantaneous (controlled) process value is calculated from the physical ratio, multiplied by 1/s and displayed as a relative value. (see also Fig.: 26, example: standard ratio control)

#### Selecting the individual material flow rates:

For display of the individual material flow rates in physical units, the "extended operating level" must be selected. At this level, the individual inputs, e.g. INP1 for x1 and INP3 for x3 can be shown on display 2 (set-point display).

The effective Xp refers to the process value range  $(x_0...x_{100})$  of input x1



# 7.2.3 Example for standard ratio control:

Standard ratio control at the example of a stoichiometric combustion.



Stöchiometric combustion

Set-point Weff effective as a relative ratio is multiplied by

the stoichiometric factor s (e.g. s = 10) (**L**. I I I) so that a "stoichiometric" flow ratio can be used for calculation of the control deviation. The instantaneous (controlled) process value is determined from the physical ratio, multiplied by 1/s and displayed as a relative value.

Fig.: 25





# 7.2.4 Material batching and mixing

The following examples are intended to show that various control possibilities can be used. This is necessary, since the materials to be mixed (e.g. paste) are not always directly measurable due to their consistency. Other cases may require a component to be controlled relatively to a total and not as a ratio to another component.

w = x1/x2

The first case is obvious. Almost everybody knows what happens during brewing. Yeast (x2) must be batched in a ratio to the original wort (x1). The set-point is adjusted in "% yeast", e.g. w = 3 %. The ratio inputs are scaled in equal units. The control deviation is multiplied with "s = 0,01" and calculated according to equation xw = (x1 + N0) - 0,03 x2 so that exactly 3 % of yeast are batched with xw = 0. Process value display is also in %. Constant N<sub>0</sub> is without importance (N<sub>0</sub> = 0).





Fig.: 27 Ratio control = x1/(x1+x2)





Unlike the previous examples, yoghurt (x2) and the final product (x1) are measured in this case.



Fig.: 28 Ratio control =  $(x^2 - x^1 + N^0) / x^2$ 



# 7.3 Three-element control

With three-element control, process value calculation is according to equation

$$x = x1 + \underline{a} \cdot (x2 - x3)$$
 (Para  $\rightarrow$  Input  $\rightarrow$  IstW  $\rightarrow$  a)

whereby term  $(x^2 - x^3)$  is the difference between the steam and water flow rates.

Factor b for flow range matching used so far is omitted, because the mA signals are directly converted into physical units during input value processing  $(x_0, x_{100})$ .

Main variable x1 (level) is displayed on the process value display, however, switch-over to calculated process value x is possible at the extended operating level (start-up and set-up).

For selecting a three-element controller, the  $L \pm \Im P = 2$  in L.  $\square \square$  must be entered.



Fig.: 30 Block diagram for three-element control



# 7.4 Mean value

For controlling a process purposefully, the correct process value (for the product) must be used. When measuring e.g. the temperatures at two different points in a furnace, mean value formation can be used for process value determination.

The mean value is calculated according to equation: x = (1 - b) x1 + bx2.

Parameter b can be used for determining a weight ratio for the two signals. If b = 0.5 is entered, the arithmetic mean value is calculated.

Fig.: 31 Mean value formation (furnace)



# 8 Correcting variable processing

The following considerations in connection with correcting variable processing are valid for continuous controllers, two-point, three-point and three-point stepping controllers. The following diagram shows the functions and interactions of correcting variable processing.





# 8.1 Second correcting value

Similar to set-point processing, switch-over to a second preset correcting value Y2 is possible. The signal source for y/Y2 switch-over must be selected with [ 19 ].

Whether Y2 has safety functions, or whether it is only a pre-defined start position in defined process conditions is determined only by the use and integration into an automation concept.  $Y2 \rightarrow Y$  switch-over is bumpless.

# 8.2 Correcting variable limits

Parameters Ymin and Ymax determine the limits of the correcting variable range within 0...100 %. With three-point and continuous controller "split range", the correcting variable limits are within -100 ... +100 %. The minimum separation of Ymin and Ymax is one digit.

Fixed correcting variable limits are specified with parameters ymin and ymax.



#### **External correcting variable limiting (override control)** 8.3

Either the lowest (OVC-) or the highest correcting value (OVC+) can be limited by an external current signal (INP4) (**L**. 105). Override control is used where bumpless switch-over to another controller when reaching defined process conditions, mainly according to other criteria, is required. The basic principle is that two controllers act on the same motor actuator.

Fig.: 34 Maximum value limiting





# 8.4 Override control

#### Override control with continuous output 8.4.1

Limiting control with three-point stepping output is possible by configuring a "continuous controller with  $(\mathbf{\hat{r}})$ position control" ( $\rightarrow$  section page 71) and by limiting the correcting variable via INP4 ( $\rightarrow$  section 8.3). For this, option card "C" is required.

KS 9x e.g. furnace temperature INP4 limiting controlle KS 94 OVC + / -INP e.g. product temperature OUT1 master controlle INPE OUT2 SHUT

Fig.: 36 Override control with continuous output

#### 8.4.2 Override control with three-point stepping output

Override control with three-point stepping output can be realized in the same way, by configuring a "continuous controller with position control" (**[.** | **[**]]).

Override control is also possible using a classical three-point stepping controller, however, option "C" is required for this limited controller. The positioning signals of the limiting controller must be connected as shown in Fig.: 37 opposite.

Selection which of the two controllers is activated in the process is made by the logic of the slave controller. The first "CLOSED pulse" coming from the limiting controller switches over to override control. The limited controller will be re-activated automatically, when further closing of the motor is required for the first time.

Via additional analog output OUT3 (option C), the motor position can also be transmitted as a mA signal to and displayed on the master controller.



Fig.: 37 Override control with 3-point stepping controllers

# 8.5 Bumpless A/M switch-over

Sudden process interventions by control mode switch-over are usually not desired. Excepted is purposeful switch-over  $y \rightarrow Y2$ .

A $\rightarrow$ M switch-over is always bumpless; the last correcting value is frozen and can be changed manually. The M $\rightarrow$ A switch-over is different. Correcting value differences are compensated as follows: when switching over, the integral action of the controller is set to the correcting value Y<sub>M</sub> output last plus correcting variable portions of the controller P and D action running in the background (Y<sub>I</sub> = Y<sub>M</sub> + Y<sub>PD</sub>). Now, only the integrator, which slowly adapts the correcting variable to the stationary value according to the actual control deviation is active.

Until the D action has decayed completely, the adaption can be delayed or accelerated.

Fig.: 38 Bumpless switch-over



# **8.6** Motor actuator output action

For safety reasons, motor actuators may operate inversely, i.e. they may be self-opening in case of positioning signal failure (e.g. combustion air with furnaces). Although the process is clearly a "heating process", i.e. the controller action should be inverse, "direct" action would have to be adjusted.

Inverting motor actuators can be taken into account by reversing the action of positioning output OUT. With switching outputs (relay or logic) "direct" is the normally open and "inverse" the normally closed operating principle.

The controller output action is inverse, as usual (e.g. heating) or direct (e.g. cooling). Thereby, correcting variable display and increment/decrement keys correspond to the actual energy or mass flow direction.

Fig.: 39 Normal 'heating' - process



Fig.: 40 Normal 'cooling' - process



Fig.: 41 'Heating' process with inverting actuator



# **8.7** Positioning output switch-off

The controller positioning outputs can be switched off as a reaction to sensor error, via control input and by the timer of the real-time clock (configurable).

# 8.8 Controller output action with sensor break

Dependent of configuration, sensor break causes (L. 10 1) -positioning output switch-off -output of the lowest correcting value -output of the highest correcting value -output of the second correcting value Y2

# 8.9 Position feedback Yp:

The position feedback can be used for detection of the position e.g. of the motor actuator or of the valve. Position feedback Yp can be connected either as a potentiometric transducer or as a 0/4...20 mA standard current signal.

Analog input Yp can be configured for INP6 ( $\rightarrow$   $\xi$ . 450).

The position feedback must be calibrated. This can be done in two steps for  $X_0$  or  $X_{100}$ .

• Calibration for X<sub>0</sub>:

Select  $\times \square \square$  as shown in Fig. below Press the selector key, the " $\square$ " on the display  $\times \square \square$  starts blinking. Now, bring the potentiometric transducer into the position for X<sub>0</sub> (usually lower end position). The instantaneously valid value for INP6 appears on display 1. Press the selector key again to store this actual value as X0.

• Calibration for X<sub>100</sub> must be done accordingly.

Select  $\times 100$  c. Press the selector key. The "c" of the display  $\times 100$  c starts blinking. Now, bring the transducer into the position for X<sub>100</sub> (usually upper end position). The instantaneously valid value for INP6 is shown on display 1. Press the selector key again to store this actual value as X<sub>100</sub>.

Fig.: 42 Selecting parameter x0c / x100c



#### Position feedback yP as a potentiometric transducer

As a potentiometric transducer, a potentiometer is connected mechanically to the potentiometer. The potentiometer must be connected to the controller terminals. Energization is via terminals 0 % and 100 %. The voltage proportional to the motor actuator position is tapped via terminal yp. Resistance Rtotal, inclusive of lead resistances, must not exceed 1k[.

#### Position feedback yP as a 0/4...20 mA standard current signal

The input resistance is 50 [.

# **9** Special Functions

# 9.1 Control using a disturbance signal

Control with measurable disturbances z is used to improve the dynamic behaviour of slow processes with long delay times. It is configurable (C105) and can act either on the controlled process value or directly on the correcting variable without consideration of the control behaviour. Option C (INP 3) is required.

The pre-processed disturbance variable (Func1, Func2) can be used directly or after differentiation (parameter T<sub>dz</sub>), whereby either both output actions, or only one are taken into account. Fig.: 43



### 9.1.1 Yp signal

According to the latest standard of information, there are two reasons for using the position feedback (control with three-point stepping output).

In some installations, the controlled process value must be lowered by several percent with increasing load. The reduction is identical with a "permissible tolerance".

Furthermore, advantages may be gained mainly in slow processes with long delay time (avoidance or reduction of overshoot with important load changes).

Example: steam boiler

Nominal pressure:	$P_N = 18$ bar at 50 % load
Pressure limits:	18,5 bar no load
	17,5 bar full load
Measuring range:	$020$ bar $\triangleq 420$ mA (X <sub>0</sub> , X <sub>100</sub> of INP1)

#### Solution

Three solutions are possible. All required functions are provided as standard.

Simulation of an increased process value

yp (INP 6) is calibrated as usual  $(X_0, X_{100})$  and displayed as a position. As with every input, two-phase pre-processing is also provided in INP6. L. 105 selects auxiliary variable z via INP6 (with or without differentiation).

Scaling mx+b is used to calculate the correction characteristic (for **lowering** the set-point, a positive m and a negative b must be adjusted):

m = (18.5 - 17.5) bar / 100 % = 0.01b = -1bar

#### Lowering the set-point

As above, but "set-point/cascade with external offset dWe (L. 100)" is set. L. 180 selects the INP6 as source of dWe. As the correction characteristic acts on the set-point, the polarity of m and b must be reversed. In this case, differentiation is not possible.

= -0.01 m b

= +1 bar

#### Position feedback as standard signal

With yp measured via an external transmitter, connection of the current signal either as auxiliary variable z or as external set-point offset dWe to the relevant inputs and scaling it directly to the required correction range (z.B. 0...100 % = + 1...-1 bar) with X<sub>0</sub>/X<sub>100</sub> is possible.



Fig.: 45 Block diagram for Yp signal



# 9.2 "Rapid Recovery"

After short-term mains failure or plant trouble, the process might have deviated from its working point only minimally. With controller start without previous knowledge, the working point will be redetermined by evaluating the control deviation. As the control deviation might be very small, this will take rather a long time, i.e. there will be a "drop". If the controller knows its old working point, start is possible using the right correcting variable for this working point, i.e. the working point will be reached again much earlier.

This is ensured by the "Rapid Recovery" function, which is divided into two independent functions. Function "Y storage and Y tracking" ensures the approach to the correcting variable required for the working point. With higher deviations of the control variable from the target set-point, function "X tracking" ensures smooth set-point line-out to the target set-point starting from the actual control variable.



### 9.2.1 Y storage

For this, the controller continuously stores data on the actual working point (correcting variable, control variable, target set-point) in the capacitor-buffered RAM, which even provides back-up with mains failure of more than 6 hours. After mains failure or plant trouble, safe data on the working point are available. These data will be used by the controller to return to the working point sooner.

After power failure or plant disturbance, the controller goes to the correcting variable of the old working point automatically and starts controlling at the correcting variable. This is of particular advantage especially with three-point stepping controllers.

This function will show good results, if the interruption was "short". As the term "short" must be considered in relation to the process time behaviour, however, the change of process value and set-point up to which Y calibration is required after power failure can be adjusted via the parameters. This is done using new parameter XwOnY. With three-point stepping controller without position feedback and signallers, this function is not provided!

Parameter	Range	Default
XwOnY	, 099999	(function switched off)

"Y calibration is done with:  $\{x < XwOnY and \{w < XwOnY\}$ 

#### 9.2.2 Set-point ramp after switch-on

The second rapid recovery sub-function is the set-point ramp. If the process value still deviates from the set-point by a value exceeding the adjustable parameter **XwOnX** after controller enabling (according to configuration **£** 19 1; **5 £ o F f** = On  $\rightarrow$  see page 102 ), control to the set-point is via parameter GrwOn.

Parameter	Range	Default
XwOnX	, 099999	(function switched off)
GrwOn	, 099999	(function switched off)

A set-point ramp is activated when: xw > XwOnX

# 9.3 DAC<sup>®</sup> = Actuator monitoring

"DAC® ensures operating safety **D**igital Actor Control monitors the actuator safety and detects problems before there would be an increased control deviation. Monitoring is done for blockage, defective motor or capacitor or for other actuator problems affecting its function. The DAC function is available for three-point stepping controllers with position feedback, continuous controllers with position control and continuous controllers with position feedback."

# Introduction

With all controller types featuring position feedback Yp, the motor actuator can be monitored for functional troubles. With these controllers (Cfunc = 08, 09, 12), the actuator function is monitored completely. Monitoring is possible for:

- defective motor
- faulty phase sequence,
- defective motor capacitor (faulty rotary direction),
- defective power transmission to spindle or gearing,
- excessive backlash due to wear,
- jammed control valve due to e.g. foreign bodies.

The function can be enabled via parameter  $\mathsf{DAC}\mathbb{R}$  :

DAC 0: no DAC

1: DAC function checking

# Description

Unless correct Yp change detection is possible despite the output of closing or opening pulses, there is a trouble. The trouble is displayed and the controller goes to manual operation, i.e. no pulses are output any more.

Display	Signification	Possible causes
Block	No reaction	• blocking
		Cable break
DirEr	No reaction	Defective motor
		capacitorPhase error
		Wrong polarity
		• Controller output action error ( <b>[</b> 1 <b>00</b> )
YFail	Y <sub>p</sub> Error	Potentiometer defective or not connected

# **Signalling**

For detected actuator error signalling, a limit relay can be switched. **C600**, **C620**, **C640** and **C660** were extended by Src=24 / actuator error

# Desitioning value limiting

As already provided with the present KS 92/94 version, Yp monitoring for  $Y_{min}$  and  $Y_{max}$  remains available. When exceeding these limits, no further pulses in the relevant direction are output. The DAC® function ensures that no limits are exceeded even in case of one or several actuator or potentiometer errors. Due to the measurement cycle, however, limit exceeding by a very low value dependent of actuator speed and inertia cannot be prevented.

#### Reset after actuator error

With actuator error detection, the controller switches to "manual mode" and displays the error:



When the plant trouble was removed, the operator must inform the controller accordingly. For this, press key  $\blacktriangle$  or  $\bigtriangledown$  and/or switch the controller to "automatic mode". If the actuator error continues, the controller detects it and switches off again. In any case, the controller must be switched back to automatic mode by the operator!

# **Operating limits**

3-point stepping controller with position feedback or continuous controller with position control

- The Yp change must be higher than 2  $\Omega$  /sec or 0,1 mA/sec!Example: motor actuator with travel time Tm = 60sec  $\rightarrow$  resistance change R 120  $\Omega$
- Conductive plastics potentiometers must be used, because their reliability and linearity is much better than with wire potentiometers.
- Any change of the motor actuator movement must cause a potentiometer resistance change.
- Drives with a high backlash are detected as defective.

Continuous controllers with position feedback

• The position fed back may have a maximum deviation of 10% after filtering with T = 20sec.

### **Automatic** *Yp* – *calibration*

To facilitate operation, the automatic Yp calibration was introduced. The controller changes its output to determine the two end positions and actuator travel time  $_{Tm}$ .

- Start
- During manual operation, select parameter **SPEBL** and set it to 1.



#### • Procedure:

Y1 is activated, until no changes are measured any more via Yp. The measurement value is stored as **x0c**. Subsequently, Y2 is activated, until Yp does not change any more. This measured value is stored as **x100c**. The duration of adjustment from 0 to 100% is measured and stored as  $T_m$ . Like **x0c** and **x100c**, **YpCa1** can be marked for the extended operating level.

Display	signification	Possible causes
חדדר	Calibration error	• Potentiometer too small
i D D.U		• Not connected
CalEr <b>60</b>		• Potentiometer polarity error

#### • Operating limits:

The motor actuator must be able to withstand a short-term (3-4sec) operation close to its limits without damage! Otherwise, the operating limits specified for DAC are applicable (see above).

# **10** Alarm processing

Up to four alarms can be configured. These alarms are allocated to the individual outputs. Generally, each of the outputs OUT1, OUT2, OUT4, OUT5 (unless used by other signals) can be used for limit value or alarm signalling.

Each of the 4 limit values LIM1 ... LIM4 has 2 trigger points LimH (Max) and LimL (Min), which can be switched off indivudally (parameter "----"). The switching difference Lx5d of each trigger point is adjustable.

Fig.: 46 operating principle of relative limit contact LimH / LimL



**1** normally closed, **2** normally open (selection in **5.500** ff; **mode**). **LimL** and **LimH** correspond to values (**5.500** ff; **Src**), at which there will be an alarm.

Fig.: 47 operating principle of relative limit contact LimH / LimL



3 normally closed, 4 normally open (selection in £500 ff; **Mode**). LimL and LimH correspond to control deviations which cause the alarm.



Limit values below the set-point must be specified with negative polarity sign.

The variable to be monitored can be selected separately for each alarm via configuration: The following variables are available:

- effective process value (Limit contact)
- control deviation (Limit comperator)
- process value x1
- process value x2 Input + eventually signal pre-processing (Func  $1/2 \rightarrow$  page 26 a. 63)
- process value x3
- auxiliary variable z
- externals set-point we
- external set-point offset dWe
- effective set-point Weff
- position feedback Yp
- controller output
- override control OVC
- selectable set-point input W<sub>Sel</sub>
- pre-processed process value inputs INP1 ... INP6 (after input conditioning  $\rightarrow$  page 26 a. 63)
- net program time
- gross program time
- program rest time

The alarm function is also configurable:

- switched off
- sensor monitoring: signalling with sensor error of the selected signal source
- sensor monitoring / measurement value alarm:
- sensor monitoringg / measurement value alarm with suppression after set-point change and start-up
- Measuring value alarm
- Measuring value alarm with suppression after set-point change and start-up

## 10.1 Alarm 1 / (limit 1)

The function of this alarm is determined in configuration parameter [.500]. Alarm signalling is via output OUT4, if this was determined as 5 rc = 29 in the configuration [.590].

### 10.2 Alarm 2 / (limit 2)

The function of this alarm is determined in configuration parameter [.620]. Alarm signalling is via output OUT5, if this was determined as Src = 25 during configuration [.59].

### 10.

# 10.3 Alarm 3 / (limit 3)

The function of this alarm is determined in configuration parameter [.500]. Alarm signalling is via output OUT1, if this was determined as 5 rc = 27 by configuring [.500].

# 10.4 Alarm 4 / (limit 4)

The function of this alarm is determined in configuration parameter [.500]. Alarm signalling is via output OUT2, if 5rc = 28 was determined by configuring [.530].

# **11** Optimizing the controller

# **11.1** Process characteristics

In order to tune the controller to the process, the process characteristics must be determined. During self-tuning, these process data are determined automatically by the controller and converted into control parameters. In exceptional cases, however, manual determination of these process data may be necessary. For this, the response of process variable x after a step change of correcting variable y can be used (see Fig. 48). Usually, it is not possible to plot the complete response curve (0 to 100 %), as the process must be kept within certain limits.

The maximum rate of increase  $v_{max}$  can be determined from the values  $T_g$  and  $x_{max}$  (step from 0 to 100 %) or t and x (partial step response).



# **11.2** Controller characteristics

The control parameters can be determined from the values calculated for delay time Tu, max. rate of increase vmax, control range Xh and characteristic value K according to the formulas given below. Precise adjustment should be done as specified in the table. Increase Xp, if line-out to the set-point oscillates.

General formulas		Reference values					
Behavior	Xp[%]	Tv[s]	Tn[s]	Parameter	Control	Disturbance	Start-up behaviour
(D)PID	1,7 K	2 Tu	2 Tu	Xp bigger	stronger damping	slower line-out	slower reduction of duty cycle
PD	0,5 K	Tu	$\infty = 0000$	smaller	reduced damping	faster line-out	faster reduction of duty cycle
PI	2,6 K	0	6 Tu	Tv bigger	reduced damping	stronger reaction	earlier reduction of duty cycle
Р	К	0	$\infty = 0000$	smaller	stronger damping	weaker reaction	later reduction of duty cycle
3-point stepping controller PID			Tn bigger	stronger damping	slower line-out	slower reduction of duty cycle	
	1,7 K	Tu	2 Tu	smaller	reduced damping	faster line-out	slower reduction of duty cycle

The various control functions are adjustable with configuration parameter **L**. **100**; **CFunc**. Direct / inverse switch-over is always possible according to configuration **L**. **10**; **CMode**. The principle is shown in Fig.: 49.

Fig.: 49 Direct / inverse switch-over principle



# 11.2.1 Signallers

This configuration can be used for processes with small  $T_u$  and slow  $v_{\text{max}}.$  Control oscillations are determined by :

$$X_0 = x_{\max} \cdot \frac{T_u}{T_g} + X_{Sd} = v_{\max} \cdot T_u + X_{Sd}$$

The signal function corresponds to limit signalling, whereby the set-point is the limit value. The trigger point is symmetrical on both sides of the set-point; hysteresis  $X_{sd1}$  is adjustable.

The signaller with two outputs has an additional "pre-trigger point". The separation between this point and the set-point is adjustable using parameter LW (including polarity).



As no manual function is possible with a signaller, calibration (resistance transducer) is only possible by configuration changing e.g. for two-point controller.

Configuration		Effective controller parameters			
<b>L</b> : $III$ ; <b>CFunc</b> = 00 (signaller with 1 output)	Xsd1	Signaller switching difference	0,1 999,9		
01 (signaller with 2 outputs)	Lω	Trigger point separation of additional contact	-999 9999		
	Xsd2	Switching difference of additional contact	0,1 999,9		

# 11.2.2 Two-point controller

Cycle time  $T_1$  must be adjusted at configuration level. It corresponds to the minimum cycle time with 50 % duty cycle. For optimizing according to the control response, the hints given in Fig. 3 must be followed.



#### *PD behaviour* $(Tn = \infty)$

The working point is in the centre of proportional band  $X_{p1}$  at 50 % duty cycle. For keeping the process constant, a certain amount of energy dependent of the set-point is necessary. This results in a permanent control deviation, which will increase with higher values for  $X_{p1}$ .

#### DPID behaviour

By means of the integral action, the process is lined out without permanent offset.

The static characteristic of a two-point controller is identical with the one of the continuous controller. The difference is that a duty cycle is output instead of a linearly variable current signal (relay contact, 0/20mA logic signal or 0/24V control output).

Working point  $Y_0$  and cycle time  $T_1$  at 50% duty cycle are adjustable. The shortest step is 100ms.

Configuration		Effective controller parameters			
<b>[</b> . $III$ ; <b>CFunc</b> = 02 (two-point controller)	Y2	Additional correcting variable	-105 105 [%]		
	Ymin	min. correcting variable limiting	-105 105 [%]		
	Ymax	max. correcting variable limiting	-105 105 [%]		
	Y0	working point of correcting variable	-105 105 [%]		
	XP1	proportional band 1	0,1 999,9 [%]		
	Tn1	integral action time	0 9999 [s]		
	Tv1	derivative action time	0 9999 [s]		
	T1	switching period	0,4 999,9 [s]		
#### 11.2.3 Three-point controller

Adjust cycle times  $T_1$  and  $T_2$  at configuration level. They correspond to the minimum cycle times at 50 % duty cycle.

For optimizing according to the control response, the hints given in Fig. 3 must be followed.



#### PD/PD behaviour (Tn =)

The adjustment range reaches from 100 % heating (Y1) to 100 % cooling (Y2).

The proportional bands must be matched to the different heating and cooling rates. For keeping the process lined out, a certain amount of energy dependent of set-point is necessary. This results in a permanent offset, which will increase with higher  $X_{p(1,2)}$ .

#### DPID/DPID behaviour

By means of the integral action, the process is lined out without permanent offset.

The transition from trigger point 1 (heating) to trigger point 2 (cooling) is without neutral zone. The proportional bands must be matched to the different heating and cooling rates (Fig. 4).

The drawings in Fig.:52 show the static characteristic for inverse and direct action. Direct/inverse switch-over only causes the exchange of the outputs for "heating/cooling". The terms "heating" and "cooling" are used for all similar processes (batching acid/lye, ...). The neutral zone is adjustable separately for the trigger points ( $X_{sh1}$ ,  $X_{sh2}$ ), i.e. it need not be symmetrical on both sides of the set-point.

The type of positioning signals is selectable:

- heating switching, cooling switching
- heating continuous, cooling switching
- heating switching, cooling continuous

Combination "heating continuous" and "cooling continuous" is covered by "continuous split range".

With inverse controller output action, "heating" is allocated to output OUT1 and "cooling" is allocated to output OUT2. As the controller versions provide only OUT1 with current signal, "heating switching; cooling continuous" seems to be possible only via OUT3 (option C). With "direct" action, however, cooling is allocated to OUT1 and heating is allocated to OUT2, so that option C is not indispensable.

Configuration		effective controller parameters			
<b>[. 100 ; CFunc</b> = 03 (three-point controller		Xsh1	neutral zone (Xw > 0)	0,0 999,9 [%]	
	Heating /cooling switching)	Xsh2	neutral zone (Xw < 0)	0,0 999,9 [%]	
	04 (three-point controller heating	Y2	additional correcting variable	-105 105 [%]	
	continuous cooling switching)	Ymin	min. correcting variable limiting	-105 105 [%]	
	05 (three-point controller heating	Ymax	max. correcting variable limiting	-105 105 [%]	
switching cooling continuous		YØ	working point of correcting variable	-105 105 [%]	
		XP1	proportional band 1	0,1 999,9 [%]	
		XP2	proportional band 2	0,1 999,9 [%]	
		Tn1	integral action time	0 9999 [s]	
		Tv1	derivative action time	0 9999 [s]	
		T1	cycle time 1	0,4 999,9 [s]	
		T2	cycle time 2	0,4 999,9 [s]	

#### 11.2.4 $\Delta/Y/off$

The principle is identical with the control behaviour of a signal function with additional contact. Output OUT2 is used for switching over between " $\Delta$ " and "Y". Output OUT1 switches the heating power on and off.



Configuration	Effective controller parameters		
$\mathcal{L}$ . 100; $CFunc = 06( / Y / off function)$	LW trigger point separation of additional contact -999 9999		
	Xsd2 signaller switching difference 0,1		0,1 999,9
	Y2 additional correcting variable -105		-105 105 [%]
	Ymin min. correcting variable limiting -1		-105 105 [%]
	Ymax max. correcting variable limiting		-105 105 [%]
	XP1 proportional band1 0,1		0,1 999,9 [%]
	Tri1   integral action time   0 99		0 9999 [s]
	<b>T</b> $\cup$ <b>1</b> derivative action time 0		0 9999 [s]
	T1	cycle time 1	0,4 999,9 [s]

## 11.2.5 Three point stepping controller

In order to match the adjusted  $X_{p1}$  to the motor actuator travel time, the travel time  $T_m$  must be adjusted. The smallest positioning step of the controller is 80ms.

Dependent of configuration (L 13 1; **SPI**/**P**), the feedback can be switched off.

Adjusting the neutral zone

The neutral zone  $X_{Sh}$  can be increased with excessively frequent relay switching. Note, however, that an increased neutral zone will cause a decrease of the control sensitivity.

Therefore, we recommend to optimize switching frequency (wear of motor actuator) and control sensitivity.



Fig.: 54 Static operating principle of the three-point stepping controller

Three-point stepping controllers can be operated with or without position feedback Yp. Yp is not required for operation. Fig.: 54 show the static characteristics of the three-point stepping controller with inverse and direct configuration.

The hysteresis shown in this diagram is practically negligible, however, it can be calculated from the adjustable min. pulse length  $T_{pulse} \ge 100$ ms.

$$X_{sh} = \frac{Tpuls}{2} \cdot 0, 1 \cdot \frac{Xp}{Tm}$$

With **Tpuls** switched off, the shortest positioning step **Tpuls**' is dependent of **Tm**, **Xsh** and **Xp**. By variation of **Xsh**, the required min. pulse length **Tpuls**' can be reached:

$$X_{sh} = 12.5 \cdot Xp \cdot \frac{Tpuls}{Tm} - 0.75$$

#### **Correcting variable limit with three-point stepping controllers**

With 3-point stepping controller with position feedback, the output is limited to ymin and ymax. Checking if the Yp value is higher than ymax or lower than ymin is done exclusively. If this is the case, further closing or opening pulses are suppressed. Due to the actuator inertia and measurement of potentiometer via INP6 (800ms), the limits may be exceeded insignificantly.

Configuration	Effective controller parameters			
[. III; CFunc = 07 (Three-point stepping	Xsh	neutral zone	0,2 999,9 [%]	
controller without feedback)	Tpuls	Min. pulse length	0,1 2,0 [s]	
08 (Three-point stepping	Tm	Actuator travel time	10 9999 [s]	
controller with feedback)	Y2	additional correcting variable	-105 105 [%]	
	Ymin	min. correcting variable limiting	-105 105 [%]	
	Ymax	max. correcting variable limiting	-105 105 [%]	
	Xp1	proportional band 1	0,1 999,9 [%]	
	Tn1	integral action time	0 9999 [s]	
	Tv1	derivative action time	0 9999 [s]	

#### 11.2.6 Continuous controller

The static characteristic corresponds to the one of the already described two-point controller. The continuous controller in split-range operation is comparable to the three-point controller. The neutral zone can also be adjusted separately.



Fig.: 55 Static operating principle of continuous controller

With a continuous controller with position feedback, the actually flowing positioning current can be measured and displayed via INP6. Yp is not used either.

Maximum and minimum output current are adjustable: -y = 0...100 % (min. current)  $+y \ge -y + 10 \%$  (max. current)

The working point is adjustable  $y_0 = 0..100$  %.

In order to operate the instrument as a P or PD controller,  $T_n = -$  can be set by means of contact FB or by setting  $T_n = 0$ . For optimizing according to the control response, the hints given in Fig. 8 must be followed.



With contact FB closed, manual  $\rightarrow$  automatic and automatic  $\rightarrow$  manual switch-over is bumpless! Transition to the new correcting variable is with the adjusted integral action time T<sub>n</sub>.

Configuration	Effective controller parameters		
<b>E. IDD</b> ; <b>CFunc</b> = 10 (continuous controller)	Xsh1	neutral zone (Xw > 0)	0,0 999,9 [%]
	Xsh2	neutral zone (Xw < 0)	0,0 999,9 [%]
11 (continuous controller	Y2	additional correcting variable	-105 105 [%]
Split range)		min. correcting variable limiting	-105 105 [%]
12 (continuous controller	Ymax	max. correcting variable limiting	-105 105 [%]
with Yp feedback)	XP1	proportional band 1	0,1 999,9 [%]
	Хр2	proportional band 2	0,1 999,9 [%]
	Tn1	integral action time	0 9999 [s]
	Tv1	derivative action time	0 9999 [s]

#### 11.2.7 Continuous controller with position control

This is basically a cascade. A tracking controller with three-point stepping behaviour which operates with Yp as process value (INP6) is used with the continuous controller. The advantages of this combination are in the availability of all functions which are possible with continuous controllers, such as

- working point adjustment
- adjustable correcting variable limits
- override control
- use of a disturbance at the positioning output
- Switch-over to a second correcting value Y<sub>2</sub>

The disadvantage might be that the control availability depends on the Yp potentiometer, which is subject to wear. This fact is taken into account by automatic switch-over to three-point stepping control without position feed-back in case of potentiometer error.



Fig.: 56 Continuous controller with position controller

Configuration	Effective controller parameters		
[. III; CFunc = 09 (continuous controller	Tpuls	min. pulse lehgth	0,1 999,9 [s]
with position controller)	Tm	actuator travel time	10 9999 [s]
	Xsh1	neutral zone (Xw > 0)	0,0 999,9 [%]
	Xsh2	neutral zone (Xw < 0)	0,0 999,9 [%]
	Y2	additional correcting variable	-105 105 [%]
	Ymin	min. correcting variable limiting	-105 105 [%]
	Ymax	max. correcting variable limiting	-105 105 [%]
	XP1	proportional band 1	0,1 999,9 [%]
	Tn1	integral action time	0 9999 [s]
	Tv1	derivative action time	0 9999 [s]

## **12** Optimizing the controller

#### 12.1 Self-tuning

For determination of the optimum process parameters, self-tuning is possible. Self-tuning can be started and finished via the system menu during automatic or manual mode.



Moreover, self-tuning can always be cancelled by pressing the manual/automatic key R on the controller front.

#### Self-tuning preparations:

- Control behaviour PID,PI,PD or P can be selected by the user by switching off Tn=0 or Tv=0 before self-tuning start.
- Determine which parameter set must be optimized (POPt.).
- Determine the stable correcting variable (**\'Opt**m).
- Determine the set-point step (dyopt).
- Determine the 'process-at-rest' mode { [.100(0Cond)}.

#### 12.1.1 Process-at-rest monitoring:

Process-at-rest monitoring is at any time. The process is <sup>×</sup> at rest with the process value within a tolerance band of  $\pm \Delta X = 0.5\%$  during more than 60 seconds. When the monitored variable leaves this tolerance, the monitoring time counter is reset to zero. With e.g. PiR detected during control operation and output of a widely varying stable correcting variable **Yoptm** when starting the self-tuning, waiting until the full PiR time has elapsed is necessary.

With extended PiR monitoring, monitoring is done for a regularly varying instead of a constant process variable !

Configuration word [.700 (0Cond) can be used to



determine the mode of 'process-at-rest' detection. One of the following modes can be selected:

grad(x) = 0:

Process at rest is detected, when x is constant.

$grad(x) \le 0 = const \& inverse :$	Process at rest is detected, when x decreases regularly with a controller with inverse action.
$grad(x) \ge 0 = const \& direct :$	Process at rest is detected, when x increases regularly with a controller with direct action.
$grad(x) \neq 0$ :	Process at rest is detected, when x varies regularly. In this case, continuation of this constant change as long as identification lasts must be ensured.

#### 12.1.2 Set-point reserve:

As a pre-requisite for realization of the self-tuning procedure, the separation of set-point and process value must be higher than 10% of W0...W100 before output of the correcting variable step! The set-point reserve is realized either automatically by reduction of the correcting variable during the PiR phase or by manual set-point or process value changing (manual mode).

#### 12.1.3 Start during automatic operation:

After self-tuning start, stable correcting variable **YOFt** is output. After detection of 'process at rest' (PiR), the correcting variable step **dYOFt** is output and the parameter determination procedure is realized. The set-point can always be changed, whereby the gradient function for set-point adjustment is switched off.



#### 12.1.4 Start during manual operation



Self-tuning start during manual operation can be done only, if the controller was switched to manual mode via its front panel or via the interface.

During switch-over to manual operation, the correcting variable output last is stored as manual correcting variable. When starting the self-tuning, this correcting variable is used and output as temporary stable correcting variable. After reaching PiR, the optimization is started. Pre-requisite for optimization start is a sufficient set-point reserve ( $\rightarrow$  page 73).

**'P**rocess at **R**est' (PiR) can be reached already when starting, i.e. the waiting time is omitted. As during automatic mode, the set-point can always be adjusted.



After successful self-tuning, switch-over to automatic mode is automatic. The process characteristics are available as parameters Tu1,Vmax1. The parameters for the required control behaviour are determined on the basis of these characteristics.

If self-tuning is finished with an error  $(\overline{Hda}_F)$ , the stable correcting variable is output, until self-tuning is finished by the user via the system menu, front panel key  $\mathbb{R}$  or via the interface.

#### 12.1.5 Self-tuning procedure with heating:

(2-point, 3-point stepping, continuous controller)

After reaching 'process at rest', the process is started with a correcting variable step and Tu1 and Vmax1 are determined from the process reaction, if possible, at the reversal point of the step response.

#### 12.1.6 Self-tuning procedure with heating and cooling processes:

#### (3-point / split-range operation)

Self-tuning starts as with a "heating" process. After the self-tuning end, the controller is determined from the calculated parameters. These parameters are used for lining out to the pre-defined set-point, until PiR is reached again. For determining the "cooling" parameters, a set-point step is output, in order to determine Tu2 and Vmax2 using the step response. Based on these parameters, the parameters for split-range operation are also determined for cooling. When cancelling the cooling attempt, the parameters for 'heating' are also used for 'cooling'. Error ( $Ada_F$ ) signalling is omitted.



- When starting the optimization with a three-point stepping controller, the correcting variable is always reduced completely and **Yopt**. If the instantaneously effective correcting variable yp cannot be measured.
  - For keeping the process within safe limits, the set-point is monitored continuously for out-of-limits.



Whilst self-tuning is running, the override control function is switched off! I.e.: Ypid is within the limits for Ymin and Ymax.



With controllers, self-tuning is with function, i.e. Y2 = 0.

MS61/2	Signification or error	Possible solution	
0	No attempt was made or attempt cancell automatic.	ed by switching over to	
1	<i>Cancellation:</i> <i>Wrong action of correcting variable, X</i> <i>does not change towards W.</i>	Cancellation W X Y	Change controller output action.
2	Finished:Self-tuning was successful (rev	versal point found; safe esti	mation)
3	<b>Cancellation:</b> The process does not react or reacts too slowly (change of $\Delta X$ below 1% during 1 hour)	Cancellation W X Y	
4	Finished : (low reversal point) Cancellation: Stimulation insufficient (reversal point found; unsafe estimation)	Y Cancellation	Increase set-point stepdYopt.
5	<i>Cancellation:</i> <i>Optimization cancelled due to exceeded</i> <i>set-point risk.</i>	Y Cancellation	Increase separation of process value (X) and set-point (W) during start-up.
6	<i>Finished:</i> Optimization cancelled due to estimation).	exceeded set-point risk (re	versal point not reached so far; safe
7	<i>Cancellation:</i> <i>Insufficient output step</i> , $\Delta Y < 5\%$ .	Ymax Y	Increase YMax or reduce YOPtm.
8	<i>Cancellation:</i> Set-point reserve insufficient or set-point exceeded during PiR monitoring	Cancellation W X Y	Change stable correcting variable YOptm.

#### 12.1.7 Signification of self-tuning messages MSG1/MSG2



Unless control is functioning properly as required despite self-tuning, proceed additionally as described in section 12.2 (page 9, Optimizing empirically). Moreover, the specifications on further parameters must be taken into account.

## **12.2** Optimizing empirically

If process data are missing, empirical optimization by means of self-tuning or by manual attempts is possible. When attempting empirical optimization, the following information should be taken into account:

- Ensure that correcting variable and control variable will never reach inadmissible values!!!
- In order to have comparable results, the conditions for the attemps should be always identical.

The attempt procedure must be oriented at the target of optimization: control behaviour or disturbance behaviour.

The controller working point must be equal with the attempts.

When using the control parameters for the first time, they must be adjusted as follows:

- Xp as high as possible: to the highest adjustable value,
- Tv relatively high: max. the time needed by the process until a clear process reaction starts.
- Tn high: max. the time needed by the process for the overall reaction.

The time requirement for empirical optimization is rather high. In order to have a reasonable result within a relatively short period of time, we recommend proceeding as described below:

- (1) Adjust Tn=Tv=0 and Xp as high as possible (P controller). Reduce Xp from attempt to attempt, as long as control is sufficiently stable. If control becomes too unstable, increase Xp slightly and continue with (2).
- ② Measure the permanent control deviation: If it is sufficiently low, self-tuning is **finished successfully** (P). If it is too high, PD control is better for the process (adjust a relatively high Tv and continue with ③).
- (3) Reduce Xp from one attempt to the next one, as long as control is sufficiently stable. If control gets too unstable, continue with ④.
- (4) Reduce Tv and find out if control can be re-stabilized sufficiently. If this is the case, continue with (3), otherwise increase Xp slightly and continue with (5).
- (5) Find out if Xp was reduced considerably during procedures (3) and (4). If this is the case, continue with (6), otherwise PI control is recommendable for the process (set Tv to 0 and continue with (7)).
- (6) Measure the permanent control deviation. If it is sufficiently low, self-tuning is completed successfully (PD). If it is too high, PID control is preferable for the process (stop changing Xp and Tv and continue with ⑦).
- Adjust a high Tn value and reduce it as long as control is sufficiently stable. If control gets too instable, increase Xp slightly, and self-tuning is completed successfully (PID or PI).



Empirical optimization is improved considerably by using a recorder (or engineering tool trend function) for control variable (process value X) related to time requirement and quality and evaluation of the test results is facilitated significantly.



The method described above can be generalized only with restrictions and does not lead to a clear improvement of the control behaviour with all processes.



Changing working point (Y0), trigger point separation (Xsh) and cycle times (Tp1 and Tp2) leads to results which may or may not be satisfactory. With 3-point stepping controllers, Tm must be set to the real travel time of the connected motor actuator.

## 12.3 Selectable adaptation (only KS94)

For certain applications, matching the control parameter set to the actual process status may be reasonable. For this, KS94 is provided with max. 4 control parameter sets, which can be selected via various signals. With default configuration, only one parameter set is available (£.700; **DCntr = 0**). With **DContr =** 1/4/5/7, KS 94 switches over automatically between the max. 4 parameter sets. The switch-over points are pre-determined via adjustable

trigger points. Parameter **Dxsd** determines the hysteresis for all three switch-over functions.



Switch-over via		Description							
0	no function	only the actual parameter set is effective							
1	   control / disturbance   behaviour	parameter set 0 with control behaviour, parameter set 1 with disturbance behaviour. Disturbance behaviour is detected, when the absolute value of control deviation ( xw ) is < Trig1. Self-tuning can determine only parameter set 0 for control behaviour.							
2	Operation	Switch-over is by changing parameter ParNr (Contr $\rightarrow$ CPara $\rightarrow$ ParNr). In order to reach the parameter quickly, the parameter should be at "extended operating level"! ( $\rightarrow$ section 4.4 page 20)		•					
Switch-over is via digital inj		Switch-over is via digital inputs di8 and di9 on options card C.	di8	0	1	0	1		
3	Control inputs	Which parameter set is active with which input allocation is shown in the table opposite parameter	di9	0	0	1	1		
			Parameter	0	1	2	3		
4	Set-point (weff)	Switch-over is at adjustable trigger points of the set-point signal (see Fig.: 62)							
5 Process value (Xeff) S		Switch-over is at adjustable trigger points of the process value signal (see Fig.: 62)							
6	correcting variable(y)	Switch-over is at adjustable trigger points of the correcting variable (see Fig.: 62)							
7	control deviation (xw)	Switch-over is at adjustable trigger points of the control deviation	witch-over is at adjustable trigger points of the control deviation (see Fig.: 62)						

## 13 Programmer

#### 13.1 General

#### 13.1.1 Programmer definition

The KS9x programmer has 1 analog output and 4 control outputs (1...4) (digital). A survey of the most important features:

- 3 programs (recipes; KS92 only 1 program!) each with ...
- 1 analog output, 4 control outputs
- 20 segments
- individual segmentation
- common preset (to "time" or "segment start")
- common control commands (run, stop, reset)

Control outputs are not firmly coupled to the analog output segmentation. They are provided with individual segmentation, which is common for the control outputs. This means that number of segments and overall time (sum of segment times) of analog output and control output can be basically different.



Fig.: 62 Programmer definition

With respect to control signals and programmer visualization, the analog output is the master output. I.e. control commands act on the analog output (profile). Control outputs are forcibly tracked:

- Run/stop
- Preset and preset value (program time or segment start)
- Reset

The analog output also determines the displays:

- status (run/stop, reset, preset)
- program set-point
- actual segment no.
- elapsed times (net/gross program times; rest time)

#### 13.1.2 Segment parameter entry

The number of segments is generally fixed to 20 for all outputs. Whether all or only part of the segments are used is determined only by the entry of segment parameters (time, value). The first segment time  $T_{p_{i+1}}$ which follows on segment Seg defined last is adjusted with "----" ( $\triangleq$  -32000) and completes the entry sequence so that the request for entry is completed.



**Entry sequence** per recipe at parameter level (display 2):

- Change mode Wmode "step/ramp"
- Preset mode **Pmode** "program time/segment start"
- Number of following program **PNext**
- Bandwidth LC-
- Bandwidth LC+
- Reset value WFØ (analog output)
- Set-point profile
  - Set-points WP1 ... WP20
  - Segment times TF1 ... TF20 [min]
- Reset value DØ (control outputs)
- Control outputs 1...4
  - Set-points DP1 ... DP20

The set-points of control outputs are adjusted in one adjustment procedure using the 4 decimals of display 2 ("0" = off; "1" = on): e.g. c

End Si9nl

Input

<u>Contr</u> Tune

<u>Limit</u>

Timer

Sete

Prog

End

Recp3

Rece

€ End Disi

Anals

▲ ▼ Aux

control output $\rightarrow$	1	2	3	4
	0	1	0	1
	off	on	off	on

Segment times Td1 ... Td20 [min]

#### 13.1.3 Parameter pre-setting (default)

When configuring "programmer" for the first time ( $\mathbf{L}, \mathbf{L} \mathbf{D} \mathbf{D}$ ), all segments are at first inactive (switched off when leaving the configuration level. The programmer outputs the reset value Wp0 (factory setting = 0) and reacts only on control commands (run, preset, ...), after the parameters of at least one segment were set. A programmer the parameters of which were already set can be switched off by configuring it accordingly. With re-activation, the previously adjusted parameters are effective again.

With start (run), the programmer starts from the instantaneous process value with the gradient of the first segment. Elapsed time and rest time are matched accordingly (cf. "search mode",  $\rightarrow$  page 86).

Fig.: 63 Search mode at first segment after program start





**A** End

End

Td2Ø

D1

DØ

Tall

WP20 TP20

...

WP1

TP1

W₽0 LC+ LC-

Pnext

Pmode

Wmode

#### 13.1.4 Time display

Segment times are adjusted and displayed in full minutes without digits behind the decimal point!

Gross, net and rest time are displayed on the front panel (display 2) in hours . minutes (extended operating level  $\rightarrow$  page 88). Times above 99h.59min are rounded off and displayed in full hours; minutes are omitted. Times which refer to the past (**tBrut**, **tNet**), are rounded off to the next lower full hour. Times which refer to the future (**tRest**), are rounded off to the next higher full hour.

Rest time tRest = 55.45 = 66 h 45 min

Limit values (alarm 1...4) can act also on program time tBrut/tNet or on rest time tRest. Time-related limit values are adjusted dependent of configuration (**E.500** ff; **D**P) either

- with four digits in full hours  $e.g.: \mathbf{U} \mid \mathbf{J}\mathbf{Z} = 132 \text{ h}$ , or
- with 2 digits and two digits behind the decimal point, e.g.: 55.75 = 66 h + 45 min





#### *13.1.5 "Flat ramps"*

The algorithm for determination of the increments with ramp-shaped change mode within a segment is designed so that low set-point changes with high set-points can be realized also with high segment time (e.g. crystal growing; from ti= $600^{\circ}$ C to ti+1 =  $612^{\circ}$ C in 600h).

#### 13.1.6 Programs (recipes)

Number of selectable programs

The required program (recipe) can be selected differently (program number PNo):

- front panel operation
- serial interface
- control inputs (di6, di7)

Due to the limited number od displays and for keeping command of the operation, KS92 is only provided with **one program** of the described length.

KS94 contains max. 3 programs (recipes) with 20 segments.

Fig.: 64 Recipe selection



#### **Recipe selection**

Recipe selection can be done via front panel (extended operating level, "PNo"), serial interface or control inputs (configuration **L**. [20]). Max. 3 programs (KS94) are selectable via control inputs.

Modification of the recipe number (PNo) with already running programmer does not lead to cancellation of the instantaneous recipe. Only "reset" cancels the current recipe and leads to the start Wp0 of the new recipe.

#### Following program

- Automatic transition to the next process phase, or
- Waiting for enable (start signal)

The adjusted programs (recipes) can be selected manually or executed "as a sequence" automatically. Parameter "**PNext**" indicates the number of the program to be used for continuation of the operation after completion of the previous program (switched off; **PNext** = ' $\Box\Box$ '). Thus an overall process can be divided into max. three sections (process phases). In this case, the max. overall length of a program thus defined is 60 segments! Thus automatic repetition of one or several programs is also possible.

Control commands, operation and display relate exclusively to the instantaneously running, active program segment. The gross running time **tBrut** is the overall time (including pauses) from the start of the first program segment.





#### 13.1.7 Change mode ramp/step

Whether the set-point (analog output) change shall be a step or a ramp is determined by a common parameter **Wmode** valid for all segments of a recipe at parameter level (default: ramp).

#### • Step:

The set-point changes to value Wpi immediately at the beginning of segment Segi and remains unchanged during segment time Tpi.

• Ramp:

The set-point changes linearly within time Tpi from start value Segi (= end value Wpi-1 of the previous segment Segi-1; in the first segment = process value x) to the end value of segment Wpi. For the first segment, the following gradient is Wp1 - Wp0

applicable:  $\frac{rrp1 - r}{Tp1}$ 

#### – Gradient priority:

With configuration ramp with gradient priority, controller start-up is always followed by a search run, which may lead to a time reduction in the first segment. In general, the time is adapted at each search run and the gradient remains constant.

Time priority

In ramp with time priority configuration, controller start-up will always be followed by a search run, which may lead to a change of the start set-point in the first segment. In general, the gradient is matched with each search run and the time remains constant. Fig.: 68

#### 13.1.8 Preparation for operation and end position

Each program starts with a start position  $Wp_0$ , which is valid after resetting or setting up the programmer for the first time, until further changes are made.

With program start from the rest position, the first programmer segment starts from the instantaneous process value at the time of the start command ("ramp" with the gradients  $(Wp_1 - Wp_0) / Tp_1$ ). With step change mode, the set-point of the first segment is activated immediately.

Dependent of configuration (L. 120, PEnd) either

- the programmer uses the set-point of the last segment until further changing (Fig.: 69) or continues automatically with the following program (if a following program was entered in "PNext"), or
- goes to rest position Wp0 (Fig.: 70) or starting position of the following program (if a following program was entered in "PNext.") at program end. The program can be started either by Run (activation or de-activation of the control input or via front panel operation)) or Preset.

Reset generally leads to the start (Wp0) of the selected program (parameter PNo). Programmer RUN (START) / STOP can be input without option via di1/2 (**L 190**) or via di4 (HW option B) (configurable; **L 120**, **P5tart**):

- Start signal via di1 (or di2) di1 is a combination of control commands internal/external, reset and run and is used when di4 is not available. di1 = 0 switches the controller to internal set-point W; the programmer is reset (reset, Wp0). With di1 = 0→1: the programmer is running when the operation/interface is set to "run/start"; the controller uses program set-point Wp.
- This function is possible only with int./ext. switch-over via di1/2. It is not possible with int./ext. switch-over via the controller front panel.
- Run/stop via di4 (and timer; L. 192) The programmer runs (di4=1) and is stopped at di4=0. Operating mode internal/external remains unchanged.



















#### 13.1.9 Control signals and status messages

Control signals (reset, stop, ...) can be entered via control inputs (static) or via serial interface or via the front panel system menu (dynamic; edge-triggered) with equal priority

Run/start is required with program end with reset. If necessary, control input run/start must be switched off and on again.

The programmer stores the last status of control commands (capacitor-buffered RAM) so that operation from several points is generally possible.

<b>A</b> 1	• 1	• • .
( ontrol	cional	nriority
CONTROL	Signai	DIJUIUV
	0	r,

Priority	Description	Status			
1	Reset	1	0	0	0
2	Preset	0/1	1	0	0
3	Stop	0/1	0/1	1	0
Result		Reset	Preset	Stop	Run
0/1 = any status					

#### 13.1.10 Pre-requisites

For the following descriptions of the operating principle, the following setpoint-related pre-requisites which are already defined for controllers are applicable:

- general limitation of the rate of set-point change to the values adjusted for parameters Grw+ and Grw-. The gradients are adjustable with 3 digits behind the decimal point!
- storage of the external set-point We or of program set-point Wp (or of process value X; tracking: **L**. (**D5**: WTrac) as internal set-point W.

Tracking can be activated only when switching back to the internal set-point! The relevant conditions are configurable (**L**. **ISD**: **STrac**):

- a) Tracking not effective, or
- b) tracking generally effective with  $We \rightarrow W$  or  $Wp \rightarrow W$ , or
- c) as b), however, contact di2 or di12 is closed additionally.

#### 13.2 Changes in the program sequence Whilst the program is running, set-points and times (on-line) can be changed. Moreover, segments which were not available so far can be appended. The actual segment number remains unchanged. Unless the actual segment is changed, the relative elapsed time in the segment remains unchanged. **Past changes** A change of values and times in the past (already executed segments) is activated only after re-start (after previous reset). **Future changes** Future changes (segments which are not reached so far) are activated immediately. With changes of segment time, the "rest time" is re-calculated automatically. **Present changes** Changes of the actual segment time, which imply a step back into the past (e.g. reduction of segment time Tpi to lower values than the relative time already elapsed in this segment) cause a program step to the start value of the next segment. Set-point differences are compensated bumplessly with the gradients Grw+/Grw- already adjusted at the controller; the programmer continues running. Changes of the target value of the actual segment cause the segment gradient to be re-calculated once for this program run, in order to re-calculate the new target value in the remaining segment time. These (and all other) rates of change are limited by the pre-set set-point gradients Grw+/Grw-. With a program reset and start or with preset to an earlier time, the final segment gradient is re-calculated.

#### 13.3 Bandwidth monitoring

When leaving the bandwidth (LC+=max. limit; LC-=min. limit) the programmer is stopped. The program continues running, when the process value is again within the pre-defined bandwidth. Fig.: 71 only shows the operating principle of the static program profile. Actually, however, the curve is delayed accordingly in the stop times.

Parameter: LC+ max. limit LC- min. limit





On instruments with software option 'Programmer' bandwidth monitoring is also effective with programmer not configured (controller operation). Parameters LC- and LC+ are adjustable in the set-point parameters. Current set-point ramps (Grw+/Grw-) are stopped when leaving the band!

#### 13.4 Manual programmer operation

The function of front panel key A/M ( $\bigcirc$ ) was already defined for controller operation (adjustable in the parameters; **FKey**). The adjustment range of this parameter contains the following points:

- Rey without function
- Automatic / manual
- Wp / W (wext / wint)

Key  $\bigcirc$  switches the programmer to internal set-point W adjustable with the arrow keys and back. In this case, key  $\bigcirc$  is used for internal/external switch-over, whereby the programmer continues running in the background for the duration of "manual operation". In the programmer reset position, key  $\bigcirc$  switches over between Wp0  $\leftrightarrow$  W.

Run  $\rightarrow$  W switch-over is bumpless with the controller configured for tracking (storage of We or Wp as internal set-point W; **L**. **[I]** and **L**. **[J]**. After switching back from manual (W)  $\rightarrow$  Run, the programmer starts from the instantaneous process value and searches the end value of the segment with gradient (Wpi - Wpi-1) / Tpi active when switching back (search mode).

#### 13.5 Search mode (E. 120, Pwrup)

Search mode is started automatically after mains recovery, if the program was in run mode before mains failure and with "search mode" configured (**L**. 120; **Pwrup**).

Within the presently active segment, the program is continued at the point (time mark in future or past) at which process value and program set-point are equal. Relative program time in segment and rest time are corrected accordingly. If searching in the actual segment is not successful, the programmer behaviour is as follows (Fig.: 72, b...f):

The programmer repeats the actual segment, with:	The programmer skips the actual segment and starts at the
	beginning of the next segment, if:
the gradient = 0, or, if the gradient $> 0$ and X $>$ Wi, or	
if the gradient $> 0$ and X $<$ Wi-1, or	if the gradient < 0 and X < Wi
if the gradient $< 0$ and X $>$ Wi-1.	

Bumplessness is achieved by controller gradient limitation Grw+ / Grw-. *Fig.: 72 Automatical search mode* 



## 13.6 Behaviour after mains recovery and after removal of sensor errors

#### 13.6.1 Memory loss (RAM)

With memory loss, the last program set-point and the time elapsed so far are not available any more. Therefore, the programmer is reset in this case. The controller uses set-point Wp = Wp0 and waits for further control commands:

- Start via contact or operation (system menu / serial interface)
- Preset

#### 13.6.2 Memory (RAM) available

*The behaviour is configurable (***L. 120**, **Pwrup**):

Pwrup	Behaviour
0	The program is continued at the point of failure (Fig.: 73 c). Starting from the instantaneous process value, the
	effective set-point runs towards the program set-point with the relevant gradient Grw+/ The programmer continues
	running,, as long as bandwidth monitoring does not respond.
1	The programmer goes to manual mode (Fig.: 73 b). Despite applied control signals, the process value is stored as
	internal set-point W (with X-tracking configured) and the programmer waits for operator intervention. The program
	continues running. Without tracking, the internal set-point is effective.
2	Automatic search mode in the actual segment and program continuation (Fig.: 73 a). For unsuccessful search mode,
	see chapter !
3	Automatic search mode in the actual segment (Fig.: 73 a). With unsuccessful search mode the programmer goes to
	manual mode (Fig.: 73 b) and the process value is stored as internal set-point W (with X-tracking configured).
	Without tracking
4	Program continuation in the segment, in which the programmer would have been without power failure. This
	function requires the KS9x real-time clock! Searching (Fig.: 73 a) and program continuation are in this segment. For
	unsuccessful search mode

Fig.: 73 Behaviour after mains recovery and sensor fault





#### 13.7 Preset

Preset sets the programmer to a defined point which is determined according to (**Pmode**) by

- a segment start ("preset to segment" **Pmode**= 0), or
- by a preset program time ("preset to time" **Pmode**= 1).

Preset value and command can be preset at the extended parameter level ( $\rightarrow$  page 89) and via serial interface. Any set-point differences are removed bumplessly with the controller gradients Grw+/-.

#### 13.8 Sensor fault

With primary variable sensor fault, the programmer is stopped. After removal of sensor faults, the programmer behaviour is as after power failure ( $\rightarrow$  13.6.2).

#### 13.9 Programmer displays

#### 13.9.1 "Display 1"

The actual process value is always displayed on display 1.

#### 13.9.2 "Display 2"

The actual set-point is displayed at operating level on display 2.

At extended operating level, program times and actual programmer recipe number are displayed on display 2 (L 120; PSel = 0).

Format of "display 2": "88.59" hours . minutes

With display overflow (>99 hours) only the full hours are displayed. The minute display is omitted: " **188**"

#### 13.9.3 "Text 1"

At operating level, the selected unit is displayed in Text1. At extended operating level, the following displays relevant for the programmer can be selected ( $[\] \heartsuit$ ):

- program time **TNet**. (without pause times)
- program time **TBr·ut**. (incl. all pause times)
- rest time TRest
- recipe number **PNr**
- controller status State

#### 13.9.4 "Text 2"

#### Continuous display

The continuous display in "Text 2" is configurable ([.800; Text 2]). With program controller, the elapsed net program time TNetto can be displayed as Bargraph 0...100%. The dark part of the bargraph represents the rest time TRest, which is displayed right beside the bargraph. For TRest < 100 hours the rest time is displayed in hours • minutes. TRest > 99h is displayed in full hours.

Status indication

At extended operating level, KS94 text line "Text 2" is used as additional status display. "Text2" contains 16 characters, which are classified as follows.

	U Ve	282. 281.	8		
↓		$\checkmark$		¥	
Set-point (symbol)	Explanations	Status	Explanations	Status	Explanations
••••	Internal set-point		no bandwidth monitoring and no program activ	• • •	KS94 is in remote operation (front panel operation disabled)
We	External set-point	Band	Bandwidth monitoring has stopped programmer or set-point ramp	Loc	KS94 is in local mode (front panel operation possible)
WP XX. Y	Program set-point Segment number Program number	Grw	Set-point gradient presently limits the rate of change		
₩2	Second set-point	Run	Programmer running		
		End	Program end is reached		
		Rset	Programmer is in reset state.		
		Stop	Programmer was stopped		



#### 13.10 Programmer operation

Programmer operation (run, stop, reset, preset) is in menul via digital inputs or via interface (monitoring program).



Fig.: 74 Programmer operation via front keys

A preset time (parameter setting: Pmode = 1) can be entered in *hours* + *minutes* ( times < 99.59) or only in *hours* ( times > 99.59).

#### 13.11 Inputs and outputs, parameters, configuration



Analog inputs	Analog outputs
Process value (from controller)	Set-point Wp
Manual set-point (internal set-point W of controller)	Program time Tnet
Program selection via front panel/interface	Program time Tgross
	Rest time TRest
	Actual segment number Seg a (analog output) and Seg d (control output)
	Final value of actual segment

Control inputs	Control outputs
Run(start)/stop (static)	end
Reset (flank)	e/i (ext./int.)
Failure (Fail)	reset
ext/int	stop/run
PrNr via digital inputs	
Preset via operation	
Parameter	Configuration
Reset value Wp0	Source of program selection (control inputs, front/interface)
segment parameters Wpi / Tpi	source of run/stop signal
Change mode Wmode "step / ramp"	behaviour after program end
(valid for all segments; default: ramp)	Behaviour after mains failure
Function of A/M key FKey	Default display in "Text 2"
Bandwidth LC+	Bargraph TNetto = 0100%
Bandwidth LC-	
Preset mode Pmode "time / segment start"	
(for all outputs; default: preset to time)	
Preset value (system menu)	
Timer (parameter)	
Time (real-time clock; system menu)	l

## 14 Timer

#### 14.1 Definition

KS9x versions with built-in real-time clock (HW option B with RS422/485) can start automatically at a pre-set time. For this purpose, a time can be set (year, month, day, hour, minute): e.g. on 23/07/95 at 6.35 h

 $(\mathbf{i})$ 

The timer comprises a switch-on time (start;  $T5. \times \times$ ) and a switch-off time (stop;  $TE. \times \times$ ). Both switching times are adjusted absolutely (day ! month ! year ! hour ! minute). The switch-off time *Tstop* is generally adjustable, however, it is not evaluated with the programmer. The two trigger points can be used also for switching over w/W2, y/Y2 and for controller output switch-off (50URCE; L. (50) ff). Timers are adjusted at parameter level. When entering a start time with an actual start time < *TStart* Timer` is displayed in Text1.



#### Timer function after mains recovery

The behaviour is dependent of whether the start time or start and stop time are already exceeded at the time of mains recovery:

- *TStart* < *actual time* > *TStop* The timer output is activated immediately and the relevant action is triggered (program START)
- *TStart* < *TStop* < *actual time* The programmer is started; the stop marker does not switch! Switch-over functions w/W2, and y/Y2 and controller output switch-off are activated during approx. 1s with these functions configured.

#### **14.2** Entry of times and timers

Adjustment is sequentially via the front panel (time in the system menu, timer at parameter setting level) or via serial interface (saved in EEPROM). Adjustment can be started at any step so that year and month/day can be skipped. The entry sequence must be continued after starting. Cancelation is not possible. The values are displayed in "display 2":

- 1st step: year **1910**
- 2nd step:month day **0** 1.0 1
- 3rd step: hour minute 00.00

The time is capacitor-buffered (separate from the RAM buffer) for approx. 2 days! With memory loss, "ClckF" is displayed in Text 1.

Timer

## 15 User-defined texts

#### 15.1 Text1

With configuration **[.80]** I; **LUn it** = 99, a free text of 5 characters (all displayable 7-bit ASCII characters) can be entered via the engineering tool or via the serial interface and displayed in "Text 1".

#### 15.2 Text2

Up to 12 free texts of 16 characters each (all displayable characters from 7-bit ASCII) can be entered with the engineering tool (or via the serial interface) and displayed alternately in "Text 2" and on the continuous display.

The display in "Text 2" can be activated from two sources (configurable; **£800**, **Text2**):

- "internal status" (alarms, control outputs, recipes, bandwidth)
- Control inputs di1...di12

With several simultaneous statuses or control inputs, the relevant texts are displayed sequentially at intervals of 5s:

User text 1 ! Bargraph ! User text 2 ! Bargraph ! ... User text n ! Bargraph ! User text 1 ! ...



If the text display is triggered via control inputs di ([LBDD]), the statuses of the control inputs will be read also if they are not used for controller/programmer function control!

T	User texts (Text 2) can be activated by			
Text	status	digital inputs		
1	LIM1	di1		
2	LIM2	di2		
3	LIM3	di3		
4	LIM4	di4		
5	Control output 1	di5		
6	Control output 2	di6		
7	Control output 3	di7		
8	Control output 4	di8		
9	Program 1	di9		
10	Program 2	di10		
11	Program 3	di11		
12	Bandwidth LC+/-	di12		

# 16 Configuration

#### 16.1 General

The KS94 controller configuration for quick and easy function selection during subsequent operation is described in this section. During configuration, the required functions are selected from a large variety of available functions. The configuration determines the basic structure for solution of an application.

The configuration structure is designed so that determination of the required functions for a large number of applications is possible by adjustment of as few configuration words as possible. Moreover, the structure was designed flexible enough to permit additional configurations also for realization of special applications.

#### 16.2 **Basic structure**

The first menu level permits selection of the main configuration group. The user can be guided through all function configurations, or he can configure the specific functions

required for his application directly.

For all 'complex' main groups, a two-level configuration concept which enables the user to select the 'correct' setting for his application by defining only one configuration word was determined. If necessary, special functions can be determined separately. For the 'normal user', however, the configuration words are preset to purposeful default values! For simplification, the hierarchic configuration dialogue is structured so that the user can and must adjust only the 'required' configuration words.

The user configuration dialogue is started via selector key  $\Box$  and 'increment' / 'decrement' keys  $\blacksquare \lor$ , like with the other KS92/94 operating levels:

- Press the selector key to select menu items / input values / input positions within a 'level' and to change over to the next higher level at the end of a 'level'.
- Press the 'increment' / 'decrement' keys for returning to a lower level and for modification of input values.



The configuration structure is shown on the two following pages (16 and 17). All possible configuration words are listed. Configuration words which are irrelevant for a function are not displayed during the dialogue!

Switch-over to a selection menu is possible from anywhere during configuration by pressing key  $\square >3s$ .

End: More: Quit:	Return to configuration level Activating the More function Return to operating level
	(configuration changes are not effective)
Exit:	Return to operating level (configuration changes are effective and the controller is re-initialized).

Configuration	⇒3s Quit
level	Exit





#### 16.3 Main groups

The following main configuration groups are available for KS9x controller configuration:

Contr	Controller function	E. 100	•••	6. (39	$\rightarrow$ page 99
Sourc	Input allocation	C. 180	•••	6, (92	$\rightarrow$ page 101
Input	Input function	005.3	•••	E.487	$\rightarrow$ page 103
Outet	Output function	E.S 0 0	•••	6.597	$\rightarrow$ page 107
Alarm	Alarm function	E.600	•••	6.660	$\rightarrow$ page 111
Tune	Self-tuning	E.700			$\rightarrow$ page 112
Disp	User interface	0.800			$\rightarrow$ page 112
Aux	Additional function	6.900	•••	E.994	$\rightarrow$ page 113

The main configuration groups are structured in a hierarchical order, whereby determination of a dialogue for prompting only the really relevant configurations is possible.



#### **ENGINEERING TOOL 'ET/KS 94'**

Engineering Tool ET/KS94 permits realization of all operations which are possible via the KS94 front panel on a PC, whereby controller configuration and parameter setting are facilitated considerably.

	Configuration			×		
Engineering Tool ET/KS94	Controller Dig. Inp. Controller function (C10	Input   Output   Límit   Option   I <b>0)</b>		1	Two-point Signaller with 1 output	v
Connection to controller	Control mode :	Two-point			Signaller with 2 outputs Two-point Three-point	
Configuration	Controller type :	Standard controller			Three-point heating continuous; cooling switched Three-point heating switched; cooling continuous	
Parameters	Set-point functions :	Set-point control	-		Delta / star / off Three-point stepping Three-point stepping with position foodback Yn	
(12 Calibration	Additional configuratio	n (C101)		X	Continuous controller with 3-point output Continuous controller	
De19	Operating sense :	inverse	-		Continuous controller split range Continuous controller with feedback Yp	
	Differentiation :	on process value X	-			
	On sensor break :	y = Ymin (0%)	-			
	Options					
	Ratio control	Program control				
	<u> </u>		1 -			
		OK Cancel	<u>H</u> elp			

The engineering tool offers the following functions:

- Creation and modification of the parameter set
- Transmission of a parameter set to KS94
- Read-out of a parameter set from a KS94
- Long-term storage of various parameter sets on hard disk or floppy
- Display of operating data

Connection of PC and KS94 controller is via an RS232/TTL adaptor cable, which must be ordered separately (ordering information  $\rightarrow$  see page 43 section 12). In conjunction with the 'SIM/KS 94' controller simulation, a graphic trend display of the real process data is available!

#### **16.4** CONTR: Controller

This main group determines the controller structure and function, which is used as starting point for controller configuration for a particular application. The main controller configuration [.100] leads to an input and output pre-adjustment ([.180]..[.190], [.500]..[.59]). This 'proposal' must always be checked before commissioning and corrected, if necessary. After determination of this word, no further settings are required for a large number of applications. Additional function adaptions are possible via configuration words [.105] and the following configurations.

	Main controller configuration 1:
CON1 <b>[]2.0.0</b> Main contr. 1	

CFunc. (Control behaviour)		WFunc
$\rightarrow$ p.	V (Controller type)	
00: signaller 1 output	0: standard controller	0: set-point
01: signaller 2 outputs	1: ratio controller	1: set-point / cascade
02: 2-pnt.controller	(→C.107)	2: programmer
03: 3-pnt.controller (heating switching and cooling switching)	2: 3-element controller	3: set-point with ext. offset
04: 3-pnt.controller (heating continuous and cooling switching)	$x_{eff} = x_1 + a \cdot (x_2 - x_3)$	4: set-point / cascade with
05: 3-pnt.controller (heating switching and cooling continuous)	3: mean value	internal offset
06: $\Delta$ /Y-off	$x_{eff} = (1-b) \cdot x1 + b \cdot x2$	5: set-point / cascade with
07: 3-pnt.stepping		external offset
08: 3-pnt.stepping with Yp (INP6)		6: programmer with
09: continuous with position controler		internal offset
10: continuous		7: programmer with
11: continuous split-range (only with Optin C; OUT1 and OUT3)		external offset
12: continuous with current feedback via Yp (INP6)		

<b>CON1 D. (. (.D)</b> contr. main 2	Main controller con	nfiguration 2:
CMode	CDiff	CFail
<ul> <li>(Output action)</li> </ul>	▼ (Differentiation)	✓ (Controller behaviour with main variable sensor break)
0: inverse 1: direct	0: differentiate Xw 1: differentiate X	<ul> <li>0: neutral (controller outputs switched off)</li> <li>1: Ypid = Ymin (0)</li> <li>2: Ypid = Ymax (100)</li> <li>3: Ypid = Y2 (adjustment via front panel not possible)</li> <li>4: Ypid = Y2 (adjustment via front panel possible)</li> </ul>

More

More

More

More

More

CON1 00.00 contr. add 1	Use of an auxiliary variable and exter	nal y limiting:		г
	CAux			COVC
	(Auxiliary variable z via INP3/6)		┥	(Output limiting)
00: no	<b>↓</b>	*	0:	no external limiting
01: X+Z in conjunction	with the process value without differentiation		1:	OVC+
02: X+-dZ/dt in conjune	tion with the process value with differentiation	n in both directions	2:	OVC-
03: X+dZ/dt in conjunc	tion with the process value with differentiation	and positive change		
04: X-dZ/dt in conjunct	ion with the process value with differentiation	and negative change		
05: Y+Z in conjunction	with the correcting variable without differenti	ation		
	e			
06: Y+-dZ/dt in conjune	tion with the correcting variable with differen	tiation in both directions		
06: Y+-dZ/dt in conjune 07: Y+dZ/dt in conjune	tion with the correcting variable with different ion with the correcting variable with different	iation in both directions iation and positive change		

		1
WTrac	dW	W Sel
(Behaviour of Wint when switching over from Wext to Wint with the w tracking input switched on )	(Type of set-point ▼ tracking.)	(MIN/MAX selection)
0: Set-point tracking 1: Process value tracking	0: additive 1: factor	0: no selection 1: Max selection Weff 2: Min selection Weff

#### Ratio functions: (only with ratio controller)



CON1 contr.

	Ratio	XDP
	▼ (Ratio control function)	(Process value decimal point)
Γ	1: $(x1 + N0) / x2$	0: no digit behind decimal point
	2: $(x1 + N0) / (x1 + x2)$	1: 1 digit behind decimal point
	3: $(x2 - x1 + N0) / x2$	2: 2 digits behind decimal point
		3: 3 digits behind decimal point



#### Span start X0: (only with ratio controller)

Xmin:(min. process value limiting Xmin) Numeric value: -999 ... 9999

	E. (89	S X
Xmax max.	<b>(0.00</b> limit X	N

#### Span end X100: (only with ratio controller)

Xmax:(max. process value limiting Xmax) Numeric value: -999 ... 9999 and Xmin Xmax





Numeric value: 00.00 ... 99.99 (2 fixed digits behind decimal point)



S factor

1.88

#### Programmer configuration:

(only with programmer configured)

	7	7	7
PSel	PwrUp	PEnd	PStrt
(Source for program ▼ selection)	▼ (Behaviour with mains recovery)	$\checkmark$ (Behaviour with program end)	▼(Source for Run/Stop)
0: program selection via operation 1: program selection via control input	<ul><li>0: continue program</li><li>1: stop program and switch over to Wint</li><li>2: continue program after automatic research</li></ul>	<ul><li>0: continue with following program</li><li>1: following program and reset (start required)</li></ul>	0: start/stop and reset together <sup>1</sup> ). control with int/ext (without Option B)
<ul> <li>3: continue program after successful automatic research otherwise switch over to Wint</li> <li>4: continue program at the time mark of mains recovery</li> </ul>		1: start/stop and reset separate. (Option B)	

#### **16.5** SOURCE: Input signal allocation

Input signal allocation is dependent of main controller configuration 'L. 100 '. this proposal must always be checked before commissioning and corrected, if necessary. Therefore, input signal allocation 'SOURCE' is no independent main item and considered as additional configuration of 'CONTR'.

CON1 C. Rha Inp-alloc. Rha				
S X2 (Signal source for X2 with ratio ✓ and three-element controller)	Sluext. ▼ (Signal source for Wext with controller with external set-point)	<b>5</b> dW (Signal source for W with ▼ controller with set-point offset	5 Z (Signal source for vauxiliary variable)	
0: X2 switched off 1: X2 of INP5 2: X2 of INP3	0: Wext switched off 1: Wext of INP5 2: Wext of INP6 3: Wext of INP4	0: dW switched off 1: dW of INP5 2: dW of INP6 3: dW of INP4	0: z switched off 1: z of INP3 2: z of INP6 3: z of INP4	

<sup>1) \*[.190;</sup>  $SWi \neq e$  select the source for int/ext-switching.

CON1 CON1 CON1 CON1 CON1 CON1 CON1 CON1			
SWi∕e	STrac	SdWon	Sw∕W2
(Set-point switch-over from internal to external) <sup>1)</sup>	(Bumpless switch-over to int. set- point with int./ext. switch-over )	(Effective set-point offset)	(Switch-over to set-point w2)
<ul> <li>0: only internal set-point</li> <li>1: W/Wext via front</li> <li>2: di1=external set-point</li> <li>3: di2=external set-point</li> <li>4: di1= internal set-point</li> <li>5: di2= internal set-point</li> </ul>	0: no tracking <sup>2</sup> ) 1: tracking on 2: di2 = tracking on 3: di12 = tracking on 4: di2 = tracking off 5: di12 = tracking off	0: no offset <sup>2)</sup> 1: offset on 2: di1 = offset on 3: di2 = offset on 4: di11 = offset on 5: di1 = offset off 6: di2 = offset off 7: di11 = offset off	0: no W2 <sup>2)</sup> 1: fixed to W2 2: di1 = W2 3: di2 = W2 4: di12 = W2 5: Timer = W2 6: di1 = W 7: di2 = W 8: di12 = W



#### Allocation of digital signals for the controller functions:

	7	7	]
S A∕M	SPI/P	SY2on	SCoff
(Automatic / manual	(3.pnt.stepping controller: feedback off, otherwise PI / P switch-over)	(Output of safe ▼ correcting value)	(Switch-off controller)
0: auto/manual via front 1: fixed to manual 2: di1 = manual 3: di2 = manual 4: Backup run 5: di1 = auto 6: di2 = auto	0: PI fixed <sup>2)</sup> 1: fixed to P action 2: di1 = P action 3: di2 = P action 4: di1 = PI action 5: di2 = PI action	0: Y no Y2) <sup>2)</sup> 1: fixed to Y2 2: di1 = Y2 3: di2 = Y2 4: timer = Y2 5: di1 = Y 6: di2 = Y	<ul> <li>0: controller on/off via front (W = '')</li> <li>1: controller fixed to off</li> <li>2: di1 = controller off</li> <li>3: di2 = controller off</li> <li>4: timer= controller off</li> <li>5: di1= controller on</li> <li>6: di2= controller on</li> </ul>



More

#### Allocation of digital signals for the programmer:

(only with programmer configured)

#### SPrSt

- (Signal source for programmer run/stop) ♦
- 0: Run/Stop: Front 1: Run/Stop: di4
- 2: Run/Stop: di4 and timer 1

- 1) With programmer configured, switch-over is between internal and program set-point.
- 2) Selectable via interfaces (e.g. engineering tool; operating data)

#### **16.6 INPUT:**

The signal inputs for the previously selected controller configuration are determined in this main group. The signal inputs required for the selected controller function are displayed in the menu for configuration. As during control function configuration, a large number of applications can also be covered by determining the main configuration. At the second level, special cases can be matched and adjusted by additional, optional configuration.Max. 5 signal inputs are provided on KS94. Analog inputs INP1, INP5 and INP6 are always provided; INP3 and INP4 are optional inputs.

All analog inputs (whether or not used for control) can be used for monitoring purposes (e.g. alarm processing).

#### 16.6.1 Signal input 1 / INP1 (main variable x1)

Configuration is for main variable x1. This signal input is a universal input for which extensive functions can be configured.



#### Main configuration:

The main configuration word is used for determination of input sensor type and physical unit. Additional input configurations can be determined using the additional configuration.

	7	Г	
	Туре	Unit	DP
•	♦ (Sensor type)	(Unit) <sup>1)</sup>	
Thermocouple:	<b>Resistance thermometer:</b>	0: at <b>T'YF</b> 3040	0: no decimal point
00: Type L 0 900 °C	20: Pt 100 -99.9 850.0 °C	1: °C	1: 1 digit behind the
01: Type J 0 900 °C	21: Pt 100 -99.9 250.0 °C	2: °F	decimal point
02: Type K 0 1350 °C	25: 2 x Pt 100 -99.9 850.0 °C		2: 2 digits behind the
03: Type N 0 1300 °C	26: 2 x Pt 100 -99.9 250.0 °C		decimal point
04: Type S 0 1760 °C	Standard signals:		3: 3 digits behind decimal
05: Type R 0 1760 °C	30: 0 20 mA		point
06: Type T 0 400 °C	31: 4 20 mA		
07: Type W 0 2300°C	32: 0 10 V		only with type: 20 40
08: Type E 0 900 °C	33: 2 10 V		
09: Type B (0) 400	Potentiometric transducer:		
1820°C	40: 0 500 Ohm		



#### x0:

(physical value at 0%) numeric value -999 ... 9999 *select only with type = 30 ... 40* 



x100:

(physical value at 100%) numeric value -999 ... 9999 ,  $X0 \neq X100!$ select only with type = 30 ... 40

<sup>1)</sup> Unit settings for scaling of Typ 00...26. With Typ 30...40 the value is fixed to 0. For this case the unit to be displayed will be configured by **L80** 1.
INP1 (. (III) add. confis.	additional configuration: additional configuration, the default se ent of sensor type class.	tting for the signal input can be changed or matched
Fail	STk	XKorr
(Signal behaviour with sensor $\mathbf{v}$ fault) (Signal behaviour with sensor fault)	(Temperature compensation)	
1: upscale(X100) 2: downscale(X0) 3: XFail ( <b>£.2 †3</b> )	0: not effective 1: internal TC 2: external TC (TC fixed in <b>[.2   []</b> !)	<ul> <li>0: not effective</li> <li>1: with process value correction (adjustable via parameters ×1in,×1out,×2in,×2out)</li> </ul>
Type: 0026, 31, 40	type: 00 09	
Non-selectable digits are marked	1 by '0'	



More

## Tkref:

(external TC) numeric value:-99 ... 100 °C or °F select only with type: 00...08 and STk = 2



Tkref

external TC.

**XFail:** (substitute value with sensor error) numeric value: -999 ... 9999



### Tfm:

(filter time constant for input value processing) numeric value: 0.0 ... 999.9



#### **Optional configuration 1:**

The optional configuration can be used to determine the functions for two signal pre-processing levels.

Func1, Func2	LDP
▼▼ (Function selection for signal pre-processing)	(decimal point for gain, Xeff and yki)
0: no function, signal is output directly	0: no decimal point
1: scaling (parameters: m,b)	1: 1 digit behind the decimal point
2: linearization (segment points xs1,ys1)	2: 2 digits behind the decimal point
3: filter (parameter: Tf)	3: 3 digits behind decimal point
4: square root extraction with factor (parameter:gain)	

The Fail adjustment does not affect the controller behaviour. With sensor error, the controller behaviour is always as determined in [. [] (Cfail). The signal behaviour with sensor error acts only on a configured alarm. With a process value, x1 or INP1 alarm configured, the signal goes e.g. to the upscale value (X100) with sensor error.



Note that the input values (x-values) must be entered in ascending order. (xs1<xs2<xs3...)

The range for these configuration words is within -999 and 9999 or '----' (switched off)!



More

For limiting the number of parameters, these functions can be used only once during pre-processing levels 1 or 2! Linearization segment points which are not required can be switched off by setting '----'.

### 16.6.2 Signal input 3 / INP3 (ratio variable x2 or auxiliary variable z)

In this case, the signal is configured for ratio variable x2 or auxiliary variable z, provided that option p.c.b. C is fitted in the controller and the function was selected during controller configuration.





#### Additional configuration:

The additional configuration can be used for changing or matching the signal input default setting for the sensor type.



(Signal behaviour with sensor error)

- 1: upscale (X100) 2: downscale (X0)
- $|^{2:}$  downscale (X0 3: XFail (**L.3 (3**)

The other configuration words for INP3 are explained in section (see following table).

-	-		
X0 [.30	see	1 85.2	
X100 <b>E.3 B</b> Z	,,	585.3	
XFail 2.3 (3	,,	E1 5.3	
Tfm [2.3 / 4	,,	2.2 (4	
optional configuration 1 <b>[.320</b>	"	055.3	wit

thout linearization (Func1/2: 2)

#### 16.6.3 Signal input 4 / INP4 (variable x3, ext. set-point Wext, override control ovc+/-)

The signal for three-element variable x3 or the galvanically isolated external set-point Wext or the override control signal ovc+/- are configured with option p.c.b. C fitted in the controller and the function selected during controller configuration.

The configuration words for INP4 are explained in section and (see following table).



#### 16.6.4 Signal input 5 / INP5 (ratio variable x2, ext. set-point Wext)

The signal for ratio variable x2 or external set-point Wext is configured with option p.c.b. not fitted in the controller and the function selected during controller configuration. The configuration words for INP5 are explained in section and (see following table).



#### 16.6.5 Signal input 6 / INP6 (auxiliary variable Yp, feedback Yp)

The signal for the auxiliary variable Yp or for the position feedbackk is configured, if this was selected during controller configuration.

The configuration words for INP6 are explained in section and (see following table).

•		· · · · · · · · · · · · · · · · · · ·
Main configuration <b>E.45</b> x0 <b>E.45</b>	see	<b>C300</b> additional potentiometric transducer for Yp (type: 40)
X100 E.452	"	5.202
Additional configuration <b>E.455</b>	"	6.305
XFail 2.483	"	6.2 (3
דfm נאצע, דfm	"	C.2 (Y
Optional configuration 1	"	<b>E.220</b> without linearisierung (Func1/2: 2)

### **16.7 OUTPT:**

#### 16.7.1 Signal output 1 / OUT1

Used for configuring the source of output OUT1. This signal output is a universal output which can be configured for extensive functions.



Src Src	Туре	Mode
▼ (Signal source)	♦ (Output stage)	✓ (Motor actuator output action)
00: output switched of	0: relay (switching)	0: not selectable
01: controller output Y1/Yout1	1: 0 20 mA (continuous output)	1: direct / normally open
02: controller output Y2/Yout2	2: 4 20 mA (continuous output)	2: inverse / normally closed
03: output Ypid	3: 0 / 20 mA (logic)	
04: position feedback Yp		
05: controlling deviation Xw		
10: process value Xeff		
11: X1		
12: X2		
13: X3		
20: set-point W		
21: external set-point Wext		
22: external offset dWe		
23: set-point Weff		
24: programmer set-point Wprg		
25: alarm 1 (limit1)		
26: alarm 2 (limit2)		
27: alarm3 (limit3)		
28: alarm 1 (limit4)		

More

### [.585 1.0.0.0 OUT1

add. config

#### **Additional configuration Out1:**

Via the options configuration, the functionality for a signal post-processing stage can be determined. This configuration word is displayed only with the option enabled.

Func (Function selection for signal output processing)	DF (decimal point for xsi,x0,x100)
0: no function, signal is output	0: no decimal point
without change (0%100%)	1: 1 digit behind decimal point
1: scaling (reference values C.510	2: 2 digits behind decimal point
and C.511 are effective)	3: 3 digits behind decimal point



More



**X0:** (physical value at 0%) Numeric value -999 ... 9999



ר

x100: (physical value at 0%) Numeric value -999 ... 9999

#### Signal output 2 / OUT2 16.7.2

Used for configuring the source of output OUT2. This signal output is a universal output and can be configured for extensive functions.

C.530 OUT2 CC. ( Main config	n:	1
Src	Туре	Mode
▼ (Signal source)	(Output stage)	(Motor actuator output action)
00: output switched off	0: relay (switching)	0: not selectable
01: controller output Y1/Yout1		1: direct / normally open
02: controller output Y2/Yout2		2: inverse / normally closed
25: alarm1 (limit1)		
26: alarm2 (limit2)		
27: alarm3 (limit3)		
28: alarm4 (limit4)		

#### 16.7.3 Signal output 3 / OUT3

Used for configuring the source of output OUT3. This signal output is a universal output and can be configured for extensive functions.



### Main configuration:

Shc Туре Mode (Motor actuator output (Signal source) (Output stage) action) 00: none (output switched off) 12: process value x2 0: switched off 0: not selectable 01: controller output Y1/Yout1 13: process value x3 1: 0 ... 20 mA 1: direct / normally open 02: controller output Y2/Yout2 (continuous 20: set-point Wint 2: inverse / normally 03: controller output Ypid 21: ext. set-point Wext output) closed 04: position feedback Yp 22: ext. Offset dWe 2: 4 ... 20 mA 05: control deviation xw 23: set-point Weff (continuous 10: process value xeff 24: programmer Wprg output) 11: process value x1 3: 0 / 20 mA (logic)



### Additional configuration:

The optional configuration can be used for determining the functions for signal post-processing. This configuration word is displayed only with the option enabled.

	_	
	Func	UP
	(Function selection for signal output processing)	✓ (decimal point for xsi,x0,x100)
(	): no function, signal is output directly (0%100%)	0: no decimal point
1	: scaling (reference values <b>[.570</b> and <b>[.571</b> are effective)	1: 1 digit behind the decimal point
2	2: linearization (segment points xs1,ys1)	2: 2 digits behind the decimal point
		3: 3 digits behind decimal point



User manual KS92/94

More

More

хØ phisic. val.0%

**x0:** 

(physical value at 0%) numeric value -999 ... 9999



Note that the input values (x-values) must be entered in ascending order. (xs1<xs2<xs3...)

The configuration parameters for linearization are stored				
as follows				
572	xs1	6.573	9s1	value pair 1
6.574	xs2	E.S 75	9s2	value pair 2
6.5 76	xs3	E.S 77	ys3	value pair 3
E.S 78	xs4	E.S 79	9s4	value pair 4
6.580	xs5	E.S.8 (	ys5	value pair 5
6.582	xs6	6.583	9s6	value pair 6
6.584	xs7	6.585	9s7	value pair 7
6.586	xs8	<b>C.587</b>	ys8	value pair 8

The range for these configuration words is within -999 and 9999 or '-----' (switched off)!

### 16.7.4 Signal output 4 / OUT4

Used for configuring the source of output OUT4. This signal output can be configured for extensive functions.

OL Ma	LSSE JT4 25 ( ain confis.		ion:			1
	Sho				Туре	Mode
+	(Signal source)	•		•	(Output stage)	▼(Actuator output action)
00:	output switched off	28:	alarm 4 (limit4)	0:	relay (switching)	0: not selectable
01:	controller output Y1/Yout1	29:	programmer output 1			1: direct / normally open
02:	controller output Y2/Yout2	30:	programmer output 2			2: i nverse / normally
25:	alarm 1 (limit1)	31:	programmer output 3			closed
26:	alarm 2 (limit2)	32:	programmer output 4			
27:	alarm 3 (limit3)	33:	program end			

### 16.7.5 ignal output 5 / OUT5

Used for configuring the source of output OUT1.. This signal output can be configured for extensive functions.



↓ ↓	Src (Signal source	) 🗸	Тчре ▼ (Output stage)	Mode (Actuator output action)
00: 01: 02: 25: 26:	output switched off controller output Y1/Yout1 controller output Y2/Yout2 alarm 1 (limit1) alarm 2 (limit2)	<ul> <li>28: alarm 4 (limit4)</li> <li>29: programmer output 1</li> <li>30: programmer output 2</li> <li>31: programmer output 3</li> <li>32: programmer output 4</li> </ul>	0: relay (switching)	0: not selectable 1: direct / normally open 2: i nverse / normally closed
27:	alarm 3 (limit3)	33: program end		

### 16.7.6 DO5,6 (digital control outputs)

Additional digital control outputs are configured!



**[**.5

D06 Main conf

Ę

Main configuration: (digital control signal DO5) Selection is possible with option C fitted.

	Shc	Mode
▼	(Digital control signal DO5)	♦ (Actuator output action)
00:	output switched off	0: not selectable
01:	controller output Y1	1: direct / normally open
34:	status automatic=0 / manual=1	2: inverse / normally closed



(Digital control signal DO6) Selection is possible with option C fitted. ς H

		7
	Src	Mode
▼	(Digital control signal DO6)	<ul> <li>(Motor actuator output action)</li> </ul>
00:	output switched off	0: not selectable
02:	controller output Y2	1: direct / normally open
35:	status external=0 / internal=1	2: inverse / normally closed

### **16.8 ALARM:**

16.8.1 Alarm 1 / (limit 1)

The function for alarm 1 is configured.

<b>E.500</b> ALRM1 <b>D.0.0</b> Alarm 1	lain configuration:	7	1
	Src	Fnc	DP
(Alarm	¥ signal source)	(Alarm function)	(Decimals for alarm limits)
00: no source	12: OVC	0: no alarm (don't care)	0: no decimal point
01: Xeff	13: WMIN/MAX (Wsel)	1: sensor fail	1: 1 digit behind the
02: Xw*	14: INP1	2: sensor fail or measurement	decimal point
03: x1	16: INP3	value alarm	2: 2 digits behind the
04: x2	17: INP4	3: sensor fail or measurement value	decimal point
05: x3	18: INP5	alarm with suppression with	3: 3 digits behind the
06: auxiliary variable z	19: INP6	set-point switch-over or start-up	decimal point
07: Wext	20: program time (net)	4: measurement value alarm	-
08: $\Delta w$	21: program time (gross)	5: measurement value alarm with	
09: Weff	22: program rest time	suppression with set-point change	
10: Yp	23: Status PROFIBUS-DP	or start-up	
11: Ypid	24: faulty actor	6: Bus error (PROFIBUS-DP)	

\*Limit comparator (refered to set-point), all other versions are fitted with limit contact.

### 16.8.2 Alarm 2 (limit 2)

The function for alarm 2 is configured.

Main configuration **E.5.2** see **E.5.2** 

#### 16.8.3 Alarm 3 (limit 3)

The function for alarm 3 is configured.

Main configuration **E.5 40** see **E.500** 

Selection is possible with OUT1 configured as alarm output.

#### 16.8.4 Alarm 4 (limit 4)

The function for alarm 4 is configured.

Main configuration **E.550** see **E.500** 

Selection is possible only with OUT2 configured as alarm output

### 16.9 TUNE: self-tuning

The type of controller self-tuning and the type of controlled self-tuning can be adjusted!

Tune <b>U.U.</b> confis. Tuning	Main configuration:		
OMode (Controller ▼ self-tuning)	OCond (Process-at-rest mode)	ŪCntr (Controlled self-tuning mode)	ODP (Decimals for ▼ 0Cntr)
0: Standard	<ul> <li>0: grad = 0</li> <li>1: grad &lt; 0 with inverse controller or grad &gt; 0 with direct controller</li> <li>2: grad ≠ 0</li> </ul>	<ul> <li>0: no function</li> <li>1: selectable control / disturbance behaviour</li> <li>2: switch-over via operation</li> <li>3: switch-over via control input</li> <li>4: switch-over controlled by Weff</li> <li>5: switch-over controlled by Xeff</li> <li>6: switch-over controlled by Ypid</li> <li>7: switch-over controlled by X-W</li> </ul>	<ul> <li>0: no decimal point</li> <li>1: 1 digit behind the decimal point</li> <li>2: 2 digits behind the decimal point</li> <li>3: 3 digits behind the decimal point</li> </ul>

### <u>16.10</u> DISP: User interface for operation

Configuration of display function signification via front panel



05: bar

### 16.11 AUX: Additional functions

*16.11.1* The interface function and operating frequency for suppression of interference on inputs are configured. *COM (serial interface)* 

COM	<b>C.301</b> ADR <b>D</b> interface address	
Prot	Baud	Addr
(Interface protocol)	(Baud rate)	(Interface address)
0: 1801/4	00: not adjustable	1801/45
	01: 2400 Bd	0 99 (default 0)
	02: 4800 Bd	PROFIBUS-DP
	03: 9600 Bd	1128 (default 128)
	04: 19200 Bd	

### 16.11.2 Hardware

The hardware-related functions are configured.



### 16.11.3 Forcing signal input





FINP5	FINP6
♦ (Forcing input 5)	Forcing input 6)
0: Controller value	0: Controller
1: Forcing	value
	1: Forcing

### 16.11.4 Forcing digital input

<b>C.920</b> Fdi1 <b>D.0.0.0</b> Forcing infuts		
Fdi1	Fdi2	Fdi4
✓ (Forcing digital input 1)	♦ (Forcing digital input 2)	(Forcing digital input 4)
0: Controller value 0: Controller value		0: Controller value
1: Forcing	1: Forcing	1: Forcing

1) PROFIBUS: automatic baud rate detection

1 58.3					
Fdi5 <b>0.0.0.0</b> Forcin <del>s</del> in <del>q</del> uts		7			
Fdi5	Fdi6	Fdi7	Fdi8		
♦ (Forcing dig. input 5)	(Forcing dig. input 6)	(Forcing dig. input 7)	(Forcing dig. input 8)		
0: Controller value 1: Forcing	0: Controller value 1: Forcing	0: Controller value 1: Forcing	0: Controller value 1: Forcing		
<b>C.922</b> Fdi9 <b>0.0.0.0</b> Forcing insuts		_	7		
Fdi9 (Forcing dig. input 9)	Fdi10 (Forcing dig. input 10)	Fdi11 (Forcing dig. input 11)	Fdi12 (Forcing dig. input 12)		
0: Controller value 1: Forcing	0: Controller value 1: Forcing	0: Controller value 1: Forcing	0: Controller value 1: Forcing		
Forcing signal output					

16.11.5 FOUTS LILL FOUT1 Forcing Forcing butputs FOUT1 FOUT2 FOUT3 FOUT4 FOUT5 (Forcing signl. outp. 1) 0: Controller value 1: Forcing 1: Forcing 1: Forcing 1: Forcing 1: Forcing 2: Release signal 2: Release signal 2: Release signal 2: Release signal 2: Release signal

#### 16.11.6 Forcing digital output



### 16.11.7 Hard-/Software Codenumber

The following configuration dates are not changeable. They show the hardware version(£.991 u. £.992) and the software version (£.993 u. £.994) of the instrument.Example: 9407 923 31201Example: 4012 157 25320



### **16.12** Examples of configuration

**Block diagram** Configuration, different from default **E. IDD CFunc** = 10 (continuous) C.590 C.591 9407-9x4-xxxx Src = 25 (alarm 1) CTשך = 0 (standard controller) **Src** = 26 (alarm 2) INP1 OUT1 ≯8 0.600 WFunc = 0, 1, 4 or 5Src = 02 (xw-alarm) 30 INP5 OUT2 0.05.3 0.86.3 V/X/N T = sensor type**Src** = 03 (process value x1) INP6 >0 OUT4 C.S D D >0 C.6 4 0 Src = 01(controller output y1) **Src** = 03 (process value x1) OUT5 0.530 Src = 28 (alarm 4) Continuous controller 1 xw- alarm, 2 process value alarms **E. 100 CFunc** = 02 (2-pnt.controller) **Src** = 26 (alarm 2) 6.591 9407-9xx-xxxxx 0,66.3  $CT \Psi P = 0$  (standard controller) 5nc = 03 (process value x1) INP1 OUT1 8 E.6 4 0 WFunc = 0, 1, 4 or 55nc = 03 (process value x1) L) Ø INP5 OUT2 0.05.3 THP = sensor type INP6 >0 OUT4 0.500 → 0 Src = 01(controller output y1) OUT5 0.550 **Src** = 25 (alarm 1) 2-pnt. controller + 2 process value alarms 6.597 **E. 100 CFunc** = 03 (3-pnt.stepping) 9407-9xx-xxxxx Src = 26 (alarm 2)  $CT \Psi P = 0 \text{ (standard controller)}$ 8528.3 Src = 03 (process value x1) INP1 8 OUT1 AUF WFunc = 0, 1, 4 or 5П INP5 OUT2 0.05.3 THF = sensor type 711 INP6 >∅ OUT4 C.S 3 0 П Src = 01 (controller output y1) OUT5 C.S 9 0 5nc = 02 (controller output y2) 3-pnt. stepping controller + process value alarm f.100 CFunc = 10 (continuous) 9407-9x4-xxxx 6.530 Src = 28 (xw-alarm) 0.590 Src = 25 (alarm 1)  $CT \Psi P = 1$  (ratio controller) INP1 ¢×¢ OUT1 >8 WFunc = 0, 1, 4 or 56.591 **Src** = 26 (alarm 2) ۶Ŏ INP5 x2 OUT2 C. 180 0.06.3 Src = 02 (xw-alarm) S X2 = 1 (INP5) INP6 >0 OUT4 xeff 0.05.3 0.88.3 ->∅ THF = sensor type Src = 01 (xeff) OUT5 6.500 C.6 4 D Src = 01(controller output y1) Src = 03 (process value x1) Ratio controller (continuous) 1 xw- alarm, 2 process value alarms **E. IDD CFunc** = 10 (continuous) 0.530 9407-9x4-1x2xx 5nc = 28 (alarm 4) 6.591  $CT \Psi P = 1$  (standard controller) Src = 33 (program end) INP1 OUT1 WFunc = 3 (programmer) 0.06.3 Snc = 02 (xw-alarm) П INP5 OUT2 5.192 SPrSt = 1 (di4) Ø INP6 OUT4  $\Lambda \Lambda$ 0.02.3 Ø THP = sensor type di4 OUT5 0.00 di5 Src = 01(controller output y1) Programmer (continuous) 1 xw- alarm **E. (DD CFunc** = 11 (continuous split-range) 9407-9x4-x1xxx 0.550 5nc = 25 (alarm 1) 6.591 CTYF = 1 (standard controller) Src = 26 (alarm 2) INP1 y1 > 8 |y2 ∅ OUT1 0.06.00 WFunc = 0, 1, 4 or 55rc = 02 (xw-alarm) INP5 OUT2 v2 0.05.3 0 8 8.2 **D** THP = sensor type 5rc = 03 (process value x1) INP6 OUT4 0.00 Ø INP3 ∂ OUT5 Src = 01(controller output y1) 6.560 > 8 INP4 OUT3 Src = 02(controller output y2) Continuous contr. 'split-range'

1 xw- alarm, 1 process value alarm

### 17 Parameters

### 17.1 General

This section gives a survey of the KS92/94 parameter data and general hints for parameter handling. The parameter operation and effect on the controller operation are described with the operating principle.

The parameter setting dialogue is realized via selector key  $\Box$  and 'increment' / 'decrement' keys  $\blacksquare \lor$ , like at the other operating levels:

Press the selector key to select menu items / input values within one level and to change to the next higher level.

Press the 'increment' / 'decrement' keys to return to a lower level or to change input values.

The controller parameter structure is given on the following page. All parameters are listed. Parameters which are not relevant for a function (configuration-dependent) are not displayed!

A selection menu can be displayed anywhere at parameter level by pressing key  $\square >3s$ .

End: Mark:	return to parameter level mark the selected parameter for display at 'extended' configuration level
Exit:	return to operating level.
Conf:	transition to configuration level.



#### 17.1.1 Allocation of parameters to the 'extended operating level'

Up to 12 parameters can be allocated to the 'extended operating level' (see Fig.: 77), whereby the controller operation is simplified, since changing over to parameter level whenever one of these parameters must be changed is omitted.

Allocation: select required parameter, press 'selection' key  $\Box$  during >3s (**Para** blinks) Select Mark with 'up' key  $\blacktriangle$  and acknowledge with 'selection' key  $\Box$  (see Fig.: ).

**Delete:** select the required parameter at the extended operating level, press 'selection' key during >3s (**Fara** blinks) and acknowledge with 'up' key .

Select  $\widehat{Clear}$  and acknowledge with 'selection' key  $\bigcirc$  (see Fig.: ).

**Hold:** The Hold function can be used for selecting a parameter from the extended operating level for being visible continuously. For this, select the required parameter at the extended operating level, press 'selection' key  $\Box$  during >3s (**Para** blinks) select Hold with 'up' key  $\blacktriangle$  and confirm with 'selection' key  $\Box$  (see Fig.:).

#### **Applications:**

During optimization, frequent access to defined parameters (Xp1, Xp2, Tn and Tv) is required.

During commissioning, limit value (LimH1, LimH2, ...) or measurement value corrections must be changed frequently.

With the parameter level disabled, access to the selected parameters is possible for the operator. Deleting a parameter from the 'extended operating level' must be done at this level (see Fig.4: 78)

Fig.: 77 Marking a parameter





Fig.: 79 Survey of parameters KS92/94



### 17.2 Set-point function

Text 1	Description	Range	Default
Setpt	Set-point parameter		
LC+	Band width upper limit	09999	'' (switched off)
LC-	Band width lower limit	09999	'' (switched off)
WØ	lower set-point limit for Weff	-999 9999	0
W100	upper set-point limit for Weff	-999 9999	100
W2	additional set-point	-999 9999	100
Grw+	set-point gradient plus with W[w/min]	0.01 99.99	'' (switched off)
Grw-	set-point gradient minus with W[w/min]	0.01 99.99	'' (switched off)
Grw2	set-point gradient with W2[w/min]	0.01 99.99	'' (switched off)

### 17.3 Time function

Text 1	Description	Range	
Timer	Timer-parameters		
TS.Y	Start value: Year	0255	
TS.MD	Start value: Month and day	Month:112; Day: 131	
TS.HM	Start value: Hour and minutes	Hour:023; Minutes: 059	
TE.Y	Final value: Year	0255	
TE.MD	Final value: Month and day	Month:112; Day: 131	
TE.HM	Final value: Hour and minutes	Hour:023; Minutes: 059	

### 17.4 Programmer functions

### **Recp1** Programmer recipe 1

Analog				Digital			
Text 1	Description	Range	Def.	Text 1	Description	Range	Def.
Wmode	Change mode	0: Ramp	0	D0	Reset value control output 14	00001111	0000
		1: Step		Td1	Time segment 1	09999[min]	·
		2: Ramp (Time priority		D1	control_output 14_for_segm. 1_	00001111	0000
						L	
Pmode	Preset mode	0: Segment start	1	Td20	Time segment 20	09999[min]	<u> </u>
		1: Program time		D20	control output 14 for segm. 20	00001111	0000
Pnext	Successive program	13 or ''	<u>· · ·</u>				
LC-	Band width lower limit	09999	<u>.                                    </u>				
LC+	Band width upper limit	09999	<u>· '</u>				
WP0	Reset value W0	-9999999	0	]			
TP1	Time segment1	09999 [min]	<u> </u>				
WP1	Set-point segment 1	-9999999	0				
TP20	Time segment 20	09999 [min]	<u> </u>	]			
WP20	Set-point segment 20	-9999999	0	]			



see programmer recipe 1

Recp3

see programmer recipe 1

### 17.5 Alarm function

Text 1	Description	Range	Default
LIM1	Alarm 1		
LimL1	Low limit	-999 9999	'' (switched off)
LimH1	High limit	-999 9999	'' (switched off)
Lxsd1	Switching difference	-999 9999	0
LIM2	Alarm 2		
LimL2	Low limit	-999 9999	'' (switched off)
LimH2	High limit	-999 9999	'' (switched off)
Lxsd2	Switching difference	-999 9999	0
LIM3	Alarm 3		
LimL3	Low limit	-999 9999	'' (switched off)
LimH3	High limit	-999 9999	'' (switched off)
Lxsd3	Switching difference	-999 9999	0
LIM4	Alarm 4		
LimL4	Low limit	-999 9999	'' (switched off)
LimH4	High limit	-999 9999	'' (switched off)
Lxsd4	Switching difference	-999 9999	0

## 17.6 Self-tuning

Text 1	Description	R/W	Range	Def.
Tune	Optimization			
YOptm	Correcting variable whilst process at rest	R/W	-105 105	0
dYopt	Step width during identification	R/W	5 100	100
POpt	Parameter set to be optimized	R/W	03	1
Tri91	trigger point 1 (set $1 \leftrightarrow$ set 2)	R/W	-999 9999 (Decimal point as configured in <b>£</b> . 700; <b>ODP</b> )	
Tri92	trigger point 2 (set $2 \leftrightarrow$ set 3)	R/W	-999 9999 (Decimal point as configured in £.700; ODP)	
Tri93	trigger point 3 (set $3 \leftrightarrow$ set 4)	R/W	-999 9999 (Decimal point as configured in <b>[.100; ODP</b> )	
ORes1	Self-tuning result during heating		0: Cancellation (during optimization preparation)	
			1: Cancellation (wrong output action)	
			2: Finished (successful optimization; reversal point found)	
			3: Cancellation (process does not react or is too slow)	
			4: <b>Cancellation</b> (reversal point found; estimation unsafe)	
		R	5: <b>Cancellation</b> (reversal point not found; estimation unsafe)	
			6: Finished (optimization cancelled due to exceeded set-	
			point risk; reversal point not reached so far;	
			estimation unsafe)	
			7: <b>Cancellation</b> (correcting variable too low $\Delta Y < 5\%$ )	
			8: Cancellation (set-point reserve too low)	
ORes2	Self-tuning result during cooling	R	0 8 (see ORes1)	
Tu1	Delay time heating	R	000,0 999,9 s	
Vmax1	Vmax heating	R	000,0 999,9 /s	
Kp1	Process amplification heating	R	000,0 999,9	
Tu2	Delay time cooling	R	000,0 999,9 s	
Vmax2	Vmax cooling	R	000,0 999,9 /s	
Кр2	Process amplification cooling	R	000,0 999,9	

## 17.7 Control algorithm

Text 1 Description		Range	Default	
CPar	`a	Controller parameters		
TPu]	ls	Min. pulse length	0.1 999.9 s	0.3
Τm		Actuator response time	10 9999 s	30
Y2		Additional correcting value	-105 105 %	0
Ymin		Min. correcting variable limiting	-105 105 %	0
Yma>	<	Max. correcting variable limiting	-105 105 %	100
YØ		Correcting variable working point	-105 105 %	0
Parh	4n	Actual parameter set	0 3	
Xsd2	2	Switching difference of additional contact	0.1 999.9	1
LW		Trigger point separation of additional contact	-999 9999	0
Xsd1		Switching difference of signaller	0.1 999.9	1
Xsh2	2	Neutral zone $(Xw > 0)$	0.0 999.9 %	0
Xsh1		Neutral zone (Xw < 0)	0.0 999.9 %	0
Xsh		Neutral zone	0.2 999.9 %	0.2
	Set 0	Parameter set 0		
Xp1	0	Proportional band 1	0.1 999.9 %	100
Хр2	0	Proportional band 2	0.1 999.9 %	100
Tn1	0	Integral action time	0 9999 s	10
Tv1	0	Derivative action time	0 9999 s	10
Τ1	0	Duty cycle 1	0.4 999.9 s	5
T2	0	Duty cycle 2	0.4 999.9 s	5
	Set1	Parameter set 1		
Xp1	1	Proportional band 1	0.1 999.9 %	100
Хр2	1	Proportional band 2	0.1 999.9 %	100
Tn1	1	Integral action time	0 9999 s	10
Tv1	1	Derivative action time	0 9999 s	10
Τ1	1	Duty cycle 1	0.4 999.9 s	5
T2	1	Duty cycle 2	0.4 999.9 s	5
	Set2	Parameter set 2		
Xp1	2	Proportional band 1	0.1 999.9 %	100
Хр2	2	Proportional band 2	0.1 999.9 %	100
Tn1	2	Integral action time	0 9999 s	10
Tv1	2	Derivative action time	0 9999 s	10
Τ1	2	Duty cycle 1	0.4 999.9 s	5
T2	2	Duty cycle 2	0.4 999.9 s	5
	Set3	Parameter set 3		
Xp1	3	Proportional band 1	0.1 999.9 %	100
XP2	3	Proportional band 2	0.1 999.9 %	100
Tn1	3	Integral action time	0 9999 s	10
Tv1	3	Derivative action time	0 9999 s	10
T1	3	Duty cycle 1	0.4 999.9 s	5
T2	3	Duty cycle 2	0.4 999.9 s	5
Reco	)V	Rapid Recovery (controller on)		
XwOr	ιY	X-W limit value (X-W $\leq X \square On \square \rightarrow Y$ tracking)	0 9999 *	·,
XwOr	ηΧ	X-W limit value (X-W > XWonx $\rightarrow$ X tracking)	0 9999 *	·,
Grw0	Dn	set-point gradient with X tracking active	0,01 99,99 /min	·,

\* Decimal point position of adjustment range as for main variable X1.

# 17.8Input processing17.8.1Process value handling

	8		
Text 1	Description	Range	Default
Istw			
Tdz	Differentiation time constant for z	0 9999 s	10
NØ	Zero offset / ratio	-999 9999	0
а	Factor a / 3-element control	-999 9999	1
Ь	Factor b / mean value control	-999 9999	0.5

### 17.8.2 Signal pre-processing

Text 1	Description	Range	Default
INP1	Signal processing for INP1		
X1in	Measurement value correction	-9999999	0
X1out	Measurement value correction	-9999999	0
X2in	Meaurement value correction	-9999999	100
X2out	Measurement value correction	-9999999	100
m	Scaling: gradient m	0 9.999	1
Ь	Scaling: offset b	-999 9999	0
9ain	Square root extraction: gain	0 9.999	1
Tf	Filter: filter time constant	0 999.9 s	0.5
INP3	Signal pre-processing for INP3		
mЗ	Scaling: gradient m	0 9.999	1
b3	Scaling: offset b	-999 9999	0
9ain3	Square root extraction: gain	0 9.999	1
Tf3	Filter: filter time constant	0 999.9 s	1
INP4	Signal processing for INP4		
m4	Scaling: gradient m	0 9.999	1
b4	Scaling: offset b	-999 9999	0
9ain4	Square root extraction: gain	0 9.999	1
Tf4	Filter: filter time constant	0 999.9 s	0.5
INP5	Signal processing for INP5		
m5	Scaling: gradient m	0 9.999	1
b5	Scaling: offset b	-999 9999	0
9ain5	Square root extraction: gain	0 9.999	1
Tf5	Filter: filter time constant	0 999.9 s	0.5
INP6	Signal processing for INP6		
m6	Scaling: gradient m	0 9.999	1
b6	Scaling: offset b	-999 9999	0
9ain6	Square root extraction: gain	0 9.999	1
Tf6	Filter: filter time constant	0 999.9 s	0.5

## 17.9 Miscellaneous

Text 1	Descripti	on	Range	Range						
Aux	General									
Fkey	Function o	f front panel key 🕄.	0: no fui	nction						
	1: automatic / manual 2: Wext / Wint									
Blck1	EBloc	extended operating level	0: free	1: blocked	2: blocked by di1	3: blocked by di2	0			
	HBloc	auto/man- key	0: free	1: blocked	2: blocked by di1	3: blocked by di2	0			
	CBloc	controller off	0: free	1: blocked	2: blocked by di1	3: blocked by di2	0			
	WBloc	setpoint	0: free	1: blocked	2: blocked by di1	3: blocked by di2	0			
Blck2	PBloc	programmer preset	0: free	1: blocked	2: blocked by di1	3: blocked by di2	0			
	RBloc	programmer run/stop/reset	0: free	1: blocked	2: blocked by di1	3: blocked by di2	0			
	OBloc	selftuning	0: free	1: blocked	2: blocked by di1	3: blocked by di2	0			

## 17.10 Signals

Signl	Description	Range	Def.
Setpt	Setpoint signals		
Wint	Internal set-point		
Wext	External set-point		
dWext	External correction		
dW	Set-point offset	-99,9 999,9	0
<u>Wsel</u>	Min/max set-point		
Contr	Controller signals		
Y	Correcting value		
YP	Position feedback		
×ω	Control deviation		
$\times 1$	Main input x1		
×2	Auxillary input x2		
×3	Auxillary input x3		
z	Auxillary variable		
OVC	External correcting variable limiting		
xeff	Effectiv process value		
Input	Input signals		
INP1	Input 1		
INP1r	Raw measure 1		
INP6	Input 6		
INP6r	Raw measure 6		
Prog	Programmer signals		
WP	Programmer setpoint		
tBrut	gross time (inc. all pause times)		
tNet	net time (without pause times)		
tRest	Rest time		
PNr	Programmer no.	1 3	1
Clock	Current time		

## 18 Versions

### 18.1 Industrial controller KS92

	94079				0		1
		1	1	1		1	1
	KS 92	0					
	KS 92 with two-wire power supply	1					
POWER SUPPLY AND	230 VAC 4 relays (OUT1, OUT2, OUT4, OUT5)		0				
PROCESS OUTPUTS	230 VAC 3 relay + current/logic output (OUT1, OUT2, OUT4, OUT5)		1				
	no interface			0			
OPTION B	TTL interface and 5 control inputs (di3 di7) and 4 control outputs (do1 do4)			1			
	RS422 and 5 control inputs (di3 di7) and 4 control outputs (do1 do4) and clock			2			
	no additional function					0	
ADDITIONAL	Measured value correction					1	
1 ONCHONS	Measured value correction and programmer					2	I
	standard setting					(	)
	2-point controller					1	l
PRECONFIGURATION	3-point stepping controller					2	2
THE CONTROLLATION	Continuous controller (current/logic output required)						3
	3-point controller (logic/relay) (current/logic output required)					4	1
	Setting to specification (manual required)					9	)

### 18.2 Industrial controller KS94

	94079		$\square$	Т	Т	1
	<u> </u>	1	1	1		
	KS 94 2					
	KS 94 with two-wire power supply 3					
	90 250 VAC 4 relays (OUT1, OUT2, OUT4, OUT5)	3				
POWER SUPPLY AND	90 250 VAC 3 relays + current/logic output (OUT1, OUT2, OUT4, OUT5)	4				
PROCESS OUTPUTS	24 V UC 4 relays (OUT1, OUT2, OUT4, OUT5)	7				
	24 V UC 3 relays + current/logic output (OUT1, OUT2, OUT4, OUT5)	8				
	no interface		Ó			
	TTL-interface, 5 control-inputs (di3 di7) and 4 control-outputs (do1 do4)		1			
OPTION B	RS422, 5 control-inputs (di3 di7) 4 control-outputs (do1 do4) and Clock		2			
	PROFIBUS-DP, 5 control-inputs (di3 di7) and 4 control-outputs (do1 do4)		3			
	INTERBUS, 5 control-inputs (di3 di7) and 4 control-outputs (do1 do4)		4			
	no extension			0		
OPTION C	2 additional inputs (INP3, INP4), 1 additional output (OUT3) 5 control-inputs (di8 di12) and 2 control-outputs (do5, do6)			1		
	1 additional output OUT3			5		
	no additional function			Ó		
ADDITIONAL	measured value correction			1		
renente	measured value correction and programmer			2		
	standard setting				0	i .
	2-point controller				1	
	3-point stepping controller				2	
	continuous controller (current/logic output reqired)				3	
PRECONFIGURATION	3-point controller(logic/relay) (current/logic output reqired)				4	
	3-point stepping controller as 3-element controller (only with additional inputs INP3,INP4)				5	
	continuous controller as 3-element controller (only with additional inputs INP3,INP4)				6	
	Setting to specification (manual regired)				9	)

### **18.3** Input and output allocation with pre-configured units

The signal (e.g. X1, Y1, alarms) allocation to the inputs and outputs for the relevant pre-configuration (factory setting) is given in the following table. Allocation can be altered at any time via front panel or interface and should be corrected before commissioning, if necessary.

	Order numb	pers and pre-	configured in	nstrument fur	octions			
	<b>9407-92(0;3;7)-xxx1x</b> Two-point controller (Relayoutput)	<b>9407-92(1;4;8)-</b> xxx1x Two-point controller (logicoutput)	<b>9407-92(0;3;7)-xxx2x</b> Motor-stepping controller	<b>9407-92(1;4;8)-</b> xxx2x Motor-stepping controller	9407-92(1;4;8)-xxx3x continuous controller	<b>9407-92(1;4;8)-</b> xxx4x 3-point controller ("heating"= logic; "cooling" = relay)	<b>9407-92(3;7)-xxx5x</b> 3-point controller 3-elements controller	9407-9X(4;8)-xxx6x continuous, 3-elements controller
Inputs								
INP1					X1			
INP3					X2	-	Х	2
INP4	-						Х	3
INP5		X2; We	xt; Wd		Wext	X2; Wext; Wd	-	
INP6			Auxili	ary variable	'Z'		-	
di1					W/Wext			
di2				1	Auto/Man			
di3				Lo	cal / Remote			
di4				Progra	mmer start /s	stop		
di5				Prog	rammer rese	et		
di6				Program sel	ection / Sele	ect prg. 1		
di7				Program sel	ection / Sele	ect prg. 2		
di8				Select	parameter se	et 1		
di9				Select	parameter se	et 2		
di10				OVC+	(3-pnt steppi	ing)		
di11				OVC- (3-1	ont stepping)	w/dW		
di12					Tracking			

#### Outputs

OUT1		Y1		-	Y1					
OUT2	-	Y2			- Y2					
OUT3	OUT3									
OUT4		Alarm1			Alarm1					
OUT5		Alarm2								
do1		Programmer output 1								
do2				Progra	ammer outpu	ut 2				
do3				Progra	ammer outpu	it 3				
do4				Progra	ammer outpu	ıt 4				
do5					Auto/Man					
d06	W/Wext									

### Anti-Reset-Wind-Up

A measure which prevents the controller integrator from going into saturation

### Working pointY0

The working point of a P or PD controller indicates the correcting variable output to the process with process value = set-point. Although this value is only important for P and PD controllers, it may be of interest also with controllers with integrator (automatic working point).

### Automatic operation

Normal controller operation. The controller uses the adjusted control parameters for process control. Automatic operation is effective after switching to automatic operation (di1/di2) via a digital input AND selecting automatic operation via front-panel key 🕄. Contrary: manual operation

### **Bandwidth** control

With program control or gradient control, there may be quite important control deviations due to the process inertia. To prevent these deviations, the control deviation is monitored, in order not to exceed a preset tolerance band. As soon as the control deviation is out of the tolerance band, the set-point change is stopped.

### Three-element control

Particularly suitable for processes in which load changes would be detected too late (e.g. level control for steam boilers). In this case, a disturbance variable is used at which the mass balance (steam removal, feed water) is evaluated, subtracted and added to the control variable (after differentiation, if necessary).

### Feed-forward control

Particularly suitable for processes with long delay time, e.g. pH control. An auxiliary variable is used at which the evaluated, differentiated or delayed value of an analog input is added directly to the controller output to avoid the controller time behaviour.

### **Gradient** control

Particularly suitable for processes which do not tolerate energy shocks or quick set-point changes. Set-point changes are bumpless in both directions, because the effective set-point always runs towards the changed set-point (target set-point) by means of gradient Grw+ or Grw-. For the second set-point w2, gradient Grw2 is effective in both directions, also after switch-over  $w \rightarrow w2$ .

### Manual operation

When switching over to manual operation, the automatic control loop operation is interrupted. Transition between automatic  $\rightarrow$  manual and vice versa are bumpless. Manual operation is effective after switching over to manual via a digital input (di1/di2) OR after selecting manual operation via front-panel key 🕄 Contrary: automatic.

### Cascade control

Particularly suitable for temperature control of e.g. steam boilers. A continuous master controller (load controller) provides its output signal as an external set-point to the cascade controller, which alters the correcting variable.

### **Override** control (OVC)

Limitation of the smallest (OVC-) or of the highest (OVC+) correcting variable to the value of an analog input. This limitation control can be used e.g. if control shall be continued by another controller after reaching defined process conditions. Transition from unlimited r limited correcting variable and vice versa are bumpless.

#### See section from page

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### Program control

The effective set-point follows the programmer profile. For this, the controller must have been switched to  $w_{ext}$ .

### Process at rest

For a clear *self-tuning* attempt, the control variable must be at rest. Various rest conditions can be selected:

### Ramp function

Set-point changes are in ramps instead of stepwise. See gradient control.

### Rapid Recovery

The controller knows its working point, it can start with the right correcting variable for this working point, i.e. it will return to its working point much earlier.

### Control parameters

For optimum function, the controller must be matched to the process dynamics. The effective parameters are **Xp1**, **Tn**, **Tv** and **YO**. Dependent of controller operating principle, the following parameters can be added: **Tp1** (*with 2-point/3-point controllers*), **Xp2** and **Tp2** (*with 3-point controllers*), **Xsh** and **Tpuls** and **Tm** (*with 3-point stepping controllers*).

### Control behaviour

In general, quick line-out to the set-point without overshoot is an advantage. Dependent of process, various control behaviour types are required:

Easily controllable processes (k < 10%) can be controlled using PD controllers,

processes with (k 10...22%) can be controlled with PID controllers

 $\Box$  and difficult processes (k > 22%) can be controlled with PI controllers.

### Controller OFF

With the controller switched off, the switching outputs do not deliver any pulses and the continuous outputs are 0%.

### Self-tuning

For optimum operation, the controller must be matched to the process requirements. The time required for this can be reduced considerably, whereby the controller uses the process characteristics to determine the *control parameters* for quick line-out the set-point without overshoot.

### Soft manual

Normal manual operation: during transition from automatic r manual, the last correcting variable remains active and can be adjusted via keys  $\boxed{}$ . The transitions from automatic  $\rightarrow$  manual and vice versa are bumpless.

### Set-point switch-over

In general, the following set-points are possible: internal  $w_{int}$ , second internal set-point  $w_2$  and external set-point  $w_{ext}$ . With program control, external set-point wext must be selected. The analog set-point is provided by the programmer.

### Correcting variable

Particularly suitable for processes where load changes cause process value drops. The set-point (preferential) or process value change is load-dependent. The evaluated and filtered correcting variable is added to the set-point.

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### PI/P switch-over

During optimization of slow processes, e.g. larges furnaces, the controller I action can cause problems: after start-up optimization, line-out may take a long time. With disturbance behaviour optimization, there may be considerable overshoot. This can be prevented by switching off the I action during start-up or in case of high control deviations (e.g. by means of a limit contact which is effective for the control deviation) and by switching it on again only after the set-point was nearly reached. To prevent a permanent control deviation, the difference between limit contact and set-point must be higher than the permanent control deviation.

### Tracking

See section from page

Switching over from external or program set-point to internal set-point can cause set-point or correcting variable step changes. By using the tracking functions, transition is bumpless. Process value tracking: after switch-over, the effective process value is stored as internal set-point. Set-point tracking: after switching over, the external or program set-point used so far is stored as internal set-point.

### Ratio control

#### See section from page

Particularly suitable for control of mixtures, e.g. fuel-air mixture for ideal or stoichiometric combustion. For taking e.g. the atomizer air into account, zero offset **NO** can be added.

### X/xw differentiation

Dynamic changes of process value or set-point affect control in various ways.

- X differentiation : for better control, process value (disturbance) changes are used dynamically to improve control, i.e. the controller disturbance behaviour is used.
- Xw differentiation: Process value (disturbances) and set-point changes are used dynamically to improve the control result, i.e. in this case, the improvement is dependent of both disturbance and control behaviour.

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