# Instruction Manual 

HM 150.05 Hydrostatic
Pressure Apparatus

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HM 150.05 Hydrostatic Pressure Apparatus


## Instruction Manual

## HM 150.05 Hydrostatic Pressure Apparatus

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## HM 150.05 Hydrostatic Pressure Apparatus

## 1 <br> Introduction

The effect of hydrostatic pressure is of major significance in many areas of engineering, such as shipbuilding, the construction of dykes, weirs and locks, and in sanitary and building services engineering.

With the HM 150.05 Hydrostatic Pressure Apparatus the following key topics can be investigated by experimentation:

- Pressure distribution in a liquid taking into account gravity
- "Lateral force" of the hydrostatic pressure
- Centre of pressure of the lateral force

The appendix to this Test Instruction contains prepared worksheets which facilitate methodical evaluation of the results of the experiments.

The apparatus is designed for use in the fields of education.

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2
Unit Description


## HM 150.05 Hydrostatic Pressure Apparatus

With HM 150.05 "Hydrostatic Pressure Apparatus "the correlation between the water level and the dependent side pressure can be investigated.

The unit is of robust construction and can be set up quickly. It is therefore highly suitable for everyday use in schools and universities.

The unit can be easily transported by means of two handles.

A transparent measuring vessel with mm scale and a scale with mm increments permits precise water level and lever arm readings.

### 2.1 Commissioning

The "Hydrostatic Pressure Apparatus" should be placed on a horizontal, waterproof surface . An additional vessel for filling and emptying the water vessel should be provided.

### 2.2 Care and Maintenance

The unit and its accessories require practically no maintenance. To prevent liming, empty the unit after use and dry it with a soft cloth.

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3 Theory on the Centre of Pressure
The hydrostatic pressure of liquids is the "gravitational pressure" Phyd. It rises due to the intrinsic weight as the depth $t$ increases, and is calculated from:

$$
\begin{equation*}
p_{\text {hyd }}=\rho \cdot g \cdot t . \tag{1}
\end{equation*}
$$

$\rho$ - Density of water
g - Acceleration due to gravity ( $\mathrm{g}=9,81 \mathrm{~m} / \mathrm{s}^{2}$ )
t - Distance from liquid surface
To calculate forces acting on masonry dams or ships' hulls, for example, from the hydrostatic pressure, two steps are required:

- Reduce the pressure load on an active surface down to a resultant force $\mathrm{F}_{\mathrm{p}}$, which is applied at a point of application of force, the "centre of pressure", vertical to the active surface.
- Determine the position of this centre of pressure by determining a planar centre of force on the active surface.

It is first demonstrated how the centre of pressure can be determined. The resultant force $F_{p}$ is then calculated.

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### 3.1 Determining the Centre of Pressure



A linear pressure profile is acting on the active surface shown, because the hydrostatic pressure rises proportional to the depth $t$.

The resultant force $F_{p}$ is therefore not applied at the centre of force $C$ of the active surface, but always slightly below it, at the so-called centre of pressure D! To determine the distance e of the centre of pressure from the planar centre of force, the following model demonstration is used:

Imagine an area $A$ in front of the active surface, formed by the height $h$ and the pressure profile of the hydrostatic pressure $\mathrm{p}_{1}-\mathrm{p}_{2}$. This area is in the form of a trapezium.
The centre of pressure $D$ lies on the extension of the planarcentre of force of this area $A$. A can be broken down into partial areas $\mathrm{A}_{1}$ and $\mathrm{A}_{2}$. The respective planar centres of force are identified by black dots.

A balance of moments between the areas is then established around the point $O_{1}$ in order to find the common planar centre of force (dynamic effect in direction $\mathrm{Fp}_{\mathrm{p}}$ :

$$
\begin{equation*}
\Sigma M^{\left(O_{1}\right)}=0: A \cdot\left(\frac{h}{2}+e\right)=A_{1} \cdot \frac{h}{2}+A_{2} \cdot \frac{2 h}{3} \tag{2}
\end{equation*}
$$

Where

$$
\begin{align*}
& A_{1}=p_{1} \cdot h  \tag{3}\\
& A_{2}=\frac{p_{2}-p_{1}}{2} \cdot h \text { and }  \tag{4}\\
& A=A_{1}+A_{2} \tag{5}
\end{align*}
$$

the result is

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$$
\begin{equation*}
e=\frac{1}{6} h \cdot \frac{p_{2}-p_{1}}{p_{2}+p_{1}} \tag{6}
\end{equation*}
$$

With the hydrostatic pressure

$$
\begin{align*}
& p_{2}=\rho g \cos \alpha \cdot\left(y_{c}+\frac{h}{2}\right) \text { and }  \tag{7}\\
& p_{1}=\rho g \cos \alpha \cdot\left(y_{c}-\frac{h}{2}\right) \text { the result is } \tag{8}
\end{align*}
$$

$$
\begin{equation*}
e=\frac{1}{12} \cdot \frac{h^{2}}{y_{c}} . \tag{9}
\end{equation*}
$$

$e$ is the distance of the centre of pressure from the planar centre of force of the active surface which we are looking for.

### 3.2 Determining the Resultant Force



The hydrostatic pressure acting on the active surface can be represented as resultant force $F_{p}$, of which the line of application leads through the centre of pressure D. The size of this resultant force corresponds to the hydrostatic pressure at the planar centre of force $\mathbf{C}$ of the active surface:

$$
\begin{equation*}
p_{c}=\rho \cdot g \cdot t_{c} \tag{10}
\end{equation*}
$$

$\mathrm{p}_{\mathrm{c}}$ - Hydrostatic pressure at the planar centre of force of the active surface $t_{c}$ - Vertical distance of the planar centre of force from the surface of the liquid
In visual terms, the pressure at the planar centre of force corresponds to precisely the mean value between the highest and lowest pressure, becau-

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se of the linear pressure distribution.
If the wall is tilted by an angle $\alpha$ :

$$
\begin{equation*}
p_{c}=\rho \cdot g \cdot \cos \alpha \cdot y_{c} . \tag{11}
\end{equation*}
$$

The resultant force $F_{p}$ can now be calculated:

$$
\begin{equation*}
F_{p}=p_{c} \cdot A_{\text {active }} \tag{12}
\end{equation*}
$$

Important! To calculate the resultant force the planar centre of force of the active surface is applied, but the line of application of the resultant force $F_{p}$ runs through the centre of pressure (see section 3.1).

### 3.3 Mode of Functioning of the HM 150.05 unit



The unit's water vessel is designed as a ring segment with constant cross-section. The force due to weight $G$ of the water always produces the same moment of momentum referred to the centre of motion O as the resultant force $F_{p}$ of the active surface running through the centre of pressure D . Consequently, this apparatus can be used to determine the force of pressure $F_{p}$ and the centre of pressure.
To illustrate the point, imagine the ring segment completely filled. The force due to weight G applied to the centre of volume of the water can be broken down into two components:

- A radially applied component Gr running precisely through the centre of motion, and
- a tangential component $G_{t}$ with a lever arm $r$ acting on the centre of motion O .

The radial component $\mathrm{Gr}_{\mathrm{r}}$ exerts no momentum on centre of motion O , because its lever arm is zero. Now, regardless of the water level:

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$$
\begin{equation*}
F_{p} \cdot y_{p}=G_{i} r \tag{13}
\end{equation*}
$$

That is to say, the force due to weight $G$ of the water volume always exerts the same moment of momentum as the force $F_{p}$ at the centre of pressure D.
The derivation of (13) leads via determination of the centre of force of a ring segment and its volume.

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## 4 Experiments Relating to the Centre of Pressure

4.1 Centre of Pressure with Vertical Positioning of the Water Vessel

### 4.1.1 Performing the Experiment

### 4.1.1.1 Counterbalancing the Water Vessel



- Set the water vessel (1) to an angle of $\alpha=0^{\circ}$ using the detent (2) as shown
- Mount the rider (6), set the lever arm on the scale (e.g. $\mathrm{l}=150 \mathrm{~mm}$ )
- Counterbalance the unit with a rotating slider (3): The stop pin (4) must be precisely in the middle of the hole for this


### 4.1.1.2 Performing the Measurement

- Top up with water until the unit is balanced (stop pin (4) at centre of hole)
- Read off water level $s$ and enter it in the prepared worksheet (see Appendix)
- Increase the appended weights (7) in increments of 0.5-1 N and repeat the measurement


### 4.1.2 Evaluating the experiment

Measured values:
s-Water level reading
I- Lever arm of the force due to weight
FG - Force due to weight of the appended weights

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### 4.1.2.1 Determining the Centre of Pressure



At a water level s, below the 100 mm mark, the height of the active surface changes with the water level. If the water level is above that mark, the height of the active surface is always 100 mm .

Meaning:
s - Water level
e - Distance of centre of pressure D from planar centre of force $C$ of the active surface
$I D$ - Distance to centre of motion of the unit:
For a water level s < 100 mm :
(pressure has a triangular profile)

$$
\begin{align*}
& e=\frac{1}{6} \cdot s  \tag{1}\\
& I_{D}=200 \mathrm{~mm}-\frac{1}{3} \cdot s \tag{2}
\end{align*}
$$

For a water level s > 100 mm :
(pressure has a trapezoidal profile)

$$
\begin{align*}
& e=\frac{1}{12} \cdot \frac{(100 \mathrm{~mm})^{2}}{s-50 \mathrm{~mm}}  \tag{3}\\
& I_{D}=150 \mathrm{~mm}+e \tag{4}
\end{align*}
$$

### 4.1.2.2 Determining the Resultant Force

The resultant force corresponds to the hydrostatic pressure at the planar centre of force $C$ of the active surface. Thus, the height of water level s must again be differentiated:
Meaning:
Aact-Superficial content of active surface
$b=75 \mathrm{~mm}$ - Width of liquid vessel
$\mathrm{p}_{\mathrm{c}}$ - Hydrostat. pressure at planar centre of force

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For s < 100 mm:
(triangular profile)

$$
\begin{equation*}
p_{c}=\rho \cdot g \cdot \frac{s}{2} \text { and } A_{a c t}=s \cdot b \tag{5}
\end{equation*}
$$

For s>100 mm:
(trapezoidal profile)

$$
p_{c}=\rho \cdot g \cdot(s-50 \mathrm{~mm}) \text { and } A_{\text {act }}=100 \mathrm{~mm} \cdot b(6)
$$

The resultant force is produced as

$$
\begin{equation*}
F_{p}=p_{c} \cdot A_{\text {act }} . \tag{7}
\end{equation*}
$$

### 4.1.2.3 Balance of Moments



Calculated variables:
FG - Appended weight
I - Lever arm of appended weight referred to centre of motion O
To check the theory, a balance of moments around the centre of motion O can be established and checked:

$$
\begin{equation*}
\Sigma M^{(O)}=0: F_{G} \cdot I=F_{p} \cdot I_{D} \tag{8}
\end{equation*}
$$

### 4.2 Centre of Pressure with Water Vessel Tilted

### 4.2.1 Performing the Experiment



- Set an angle $\alpha$ and counterbalance the water vessel as described under 4.1.1.1.
- Enter the characteristic values in the prepared worksheet: Lowest water level St and highest water level sh of the active surface
- Perform the measurement as described under 4.1.1.2.


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### 4.2.2 Evaluating the experiment

The difference between evaluation of the tilted vessel and that of the vertical vessel lies in the translation of the water levels onto the tilted active surface: A factor $\cos \alpha$ must be taken into account here.

### 4.2.2.1 Determining the centre of pressure

When the water vessel is at a tilt, too, a triangular pressure profile is produced when the water level is below sh ; above that level a trapezoidal profile is produced.
Measured values:
$s$ - Water level reading
$\alpha$ - Tilt angle of vessel
Meaning:
St - Water level at lowest point of vessel
Sh - Water level of active surface at rim
e - Position of centre of pressure
h - Height of active surface
$I D$ - Distance between centre of pressure/centre of motion

For a water level s < sh a triangular profile as follows applies:

$$
\begin{align*}
& h=\frac{s-s_{t}}{\cos \alpha}  \tag{9}\\
& e=\frac{1}{6} \cdot h  \tag{10}\\
& I_{D}=200 \mathrm{~mm}-\frac{1}{3} \cdot h \tag{11}
\end{align*}
$$

For a water level s > sh a trapezoidal profile as follows applies:

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$$
\begin{align*}
& e=\frac{1}{12} \cdot \frac{(100 \mathrm{~mm})^{2}}{\frac{s-s_{t}}{\cos \alpha}-50 \mathrm{~mm}}  \tag{12}\\
& I_{D}=150 \mathrm{~mm}+e \tag{13}
\end{align*}
$$

### 4.2.2.2 Determining the resultant force


4.2.2.3 Balance of moments

The results can bechecked withthe balance of moments, as described in section 4.1.2.3.

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### 4.3 Centre of pressure with $90^{\circ}$ positioning of the water vessel

The angle $\alpha=90^{\circ}$ represents a special case. The
 resultant pressure profile has the form of a triangle, because the hydrostatic pressure is equal at every point on the active surface.
For this reason, the centre of pressure C lies precisely at the planar centre of force $D$ of the active surface

$$
\begin{equation*}
e=0 \tag{18}
\end{equation*}
$$

and has the lever arm

$$
\begin{equation*}
I_{D}=150 \mathrm{~mm} . \tag{19}
\end{equation*}
$$

The resultant force is produced as

$$
\begin{equation*}
F_{p}=\rho \cdot g \cdot\left(s-s_{t}\right) \cdot(100 \mathrm{~mm} \cdot b) \tag{20}
\end{equation*}
$$

The result can be checked with the balance of moments from section 4.1.2.3.

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### 5.2 Symbols and Units

| $\rho$ | Density of liquids | $\mathrm{g} / \mathrm{cm}^{3}$ |
| :---: | :---: | :---: |
| phyd | Hydrostatic pressure | mmHOW |
| $p_{c}$ | Hydrostatic pressure in planar centre of gravity of active surface | mmHOW |
| $F_{p}$ | Resultant force in centre of pressure | N |
| $F_{G}$ | Force due to weight of appended weights | N |
| $G$ | Force due to weight of water in measuring vessel | N |
| $h$ | Height of active surface | mm |
| $b$ | Width of liquid container | mm |
| $s$ | Water level reading/scale | mm |
| Sh | Water level at highest point of active surface | mm |
| $S_{t}$ | Water level at lowest point of measuring vessel | mm |
| $e$ | Distance between centre of pressure and planar centre of gravity | mm |
| $I D$ | Lever arm of resultant force $F_{p}$ | mm |
| 1 | Lever arm of force due to weight | mm |
| $y p$ | Distance between centre of pressure liquid level along the active surface |  |
| $y_{c}$ | Distance between planar centre of gravity and liquid level along the active surface | mm |
|  | Superficial content of active surface | $\mathrm{mm}^{2}$ |

### 5.3 Technical data

Dimensions: LxWxH $400 \times 500 \times 360 \mathrm{~mm}^{3}$
Capacity of measuring vessel:
approx. 1.8 I
Weight: approx. 10 kg

